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Dr.ing. Krishna Kanta Panthi Department of Geosciences and Petroleum krishna.panthi@ntnu.no

Aim for today's lecture is to understand;

- N T N U
- BRITTLE AND DUCTILE (PLASTIC) FAILURES
- MECHANISM OF PLASTIC DEFORMATION
- METHODS FOR ANALYSING PLASTIC DEFORMATION
 - > EMPERICAL
 - > ANALYTICAL
 - > NUMERICAL
 - > PROBABILISTIC
- SUMMARY

SOME EXAMPLES OF PLASTIC DEFORMATION





Tunnel squeezing at Modi and Kaligandaki, Nepal

SOME EXAMPLES OF PLASTIC DEFORMATION





Plastic deformation along the foliation plane of a flagstone at Headrace of Driva HPP (Norway)

SOME EXAMPLES OF PLASTIC DEFORMATION





Naptha Jhakri, India

Chamelia, Nepal



- MECHANISM OF PLASTIC DEFORMATION
- METHODS ANALYSING PLASTIC DEFORMATION
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- Fracture initiation after yielding point
- Complete failure once it reaches to Uniaxial Compression
 - Brittle failure
 - Plastic deformation (ductile) failure
- This lecture will be on the plastic deformation



Elastic – brittle (EB) failure (left) in hard rock mass; Strain softening (SS) failure (middle) in average quality rock mass and Elastic perfectly plastic (EPP) failure (right) in very poor rock mass.



MECHANISM OF PLASTIC DEFORMATION

METHODS ANALYSING PLASTIC DEFORMATION

- > EMPERICAL
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MECHANISM OF PLASTIC DEFORMATION



Remember that in many occasion insitu stresses are not isostatic! Hence, plastic deformation may be uneven as shown in previous photos!

- Re-distribution of stresses upon excavation
- Development of micro cracks in the rock mass developing viscoplastic zone
 - Time dependent inward movement of the tunnel wall and roof



DEFORMATION MECHANISM IN A ADVANCING TUNNEL



DEFORMATION MECHANISM IN A ADVANCING TUNNEL





PARAMETERS INFLUENCING PLASTIC DEFORMATION

Plastic deformation in tunnels is mainly influenced by the following parameters;

- 1. Rock mass properties
- 2. Stress conditions
- 3. Stiffness of rock support

Rock support interaction with the existing rock mass subjected to induced stresses is the key approach to be employed in analyzing plastic deformation (tunnel squeezing).



MECHANISM OF PLASTIC DEFORMATION

METHODS ANALYSING PLASTIC DEFORMATION



- > ANALYTICAL
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SUMMARY

EMPERICAL METHOD – USE OF Q-SYSTEM

| c) | Squeezing rock: plastic flow on incompetent rock under the influence of high pressure | $\sigma_{\theta} / \sigma_{c}$ | SRF |
|------------|--|--------------------------------|--------|
| 0 | Mild squeezing rock pressure | 1-5 | 5-10 |
| P | Heavy squeezing rock pressure | >5 | 10-20 |
| INOLE | mass compression strength can be estimated from $Q = 0.7\gamma Q^{1/3}$ (M density in kN/m ³ (Singh, 1993). | Pa) where γ | = rock |
| <i>d</i>) | Swelling rock: chemical swelling activity depending on the presence of water | | SRF |
| R | Mild swelling rock pressure | | 5-10 |
| S | Heavy swelling rock pressure | | 10-15 |

Weakness

- The maximum tangential stress is not relevant for squeezing (plastically deformed) rock mass.
- Low Q value does not mean rock mass squeezes.

EMPERICAL METHOD - SINGH ET AL (1992)



Weakness

> Double count of stress magnitude with H and SRF in Q



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A. CONVERGENCE CONFINEMENT METHOD

- When a tunnel is excavated, face also absorbs part of the load
- When tunnel advances, support has to carry more load as there is no 'face effect'



- Face does not advance
- No load to the support
- Ground converge (u_r⁰)
- Ground and support deform together
- Support receives part of the load that the face was carrying
- Ground converge $(u_r^{t} > u_r^{0})$
- Rock pressure to support (p_s^t)
- Face had advanced to far
- Ground-support system in equilibrium
- Support receives the final load (P_s^D)
- Ground converge to final value (u^D_r)

Carranza-Torres and Fairhurst (2000)

GRC, SCC AND LDP IN CCM



Ground reaction curve, support characteristic curve (SCC) and longitudinal deformation profile (LDP) are the basic elements of (CCM) analysis.

SOME USEFUL FORMULAE TO PLOT GRC



Carranza-Torres and Fairhurst (2000)

SOME USEFUL FORMULAE TO PLOT LDP AND SCC

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$$\frac{u_r}{u_{max}} = 0.25 + 0.75 \left[1 - \left(\frac{0.75}{0.75 + x/R} \right)^2 \right]$$

$$p_s = K_s u_r$$

$$p_i^{cr} : \text{critical initial support}$$

$$u_r^{el} : \text{Redial displacement}$$

$$\sigma_0 : \text{Far field stress}$$

$$S_0 : \text{Far field stress}$$

$$m_r : \text{rock mass material part}$$

X

- pressure re at elastic limit : rock mass material parameter III_b : Roc mass parameter S G_{rm} : Shear modulus of rock mass : Support pressure **p**_s R_{pl} : Radius of plastic zone K_{ψ} : Dilation coefficient K : Support stiffness R : Tunnel radius : Redial displacement at distance x u_r
 - : Distance to the point from the face

HOEK AND MARINOS (2000) APPROACH



HOEK AND MARINOS (2000) APPROACH





LIMITATIONS OF CCM AND HOEK & MARINOS METHOD

- Circular shape of the tunnel
- Isostatic stress conditions
- Considers only vertical gravitational stress
- Estimate only final tunnel strain (closure)

In reality

- Tunnels and caverns are mostly noncircular excluding TBM tunnels
- Stress in squeezing rock mass are seldom isostatic

$$\sigma_h = \frac{\nu}{1 - \nu} \times \sigma_V + \sigma_{tec}$$

PANTHI AND SHRESTHA (2017) APPROACH





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NUMERICAL ANALYSIS



An example of plastic deformation analysis using Phase 2 without rock support

NUMERICAL ANALYSIS



An example of plastic deformation analysis using Phase 2 with rock support

NUMERICAL ANALYSIS

N T N U

Advantage

- No limitation on the shape and size
- Considers all type of stress conditions
- Strong and fast

Disadvantage

- Quality of input variables (valid also to all other methods)
- No control on mathematical equation used in the programs
- Single point method that only looks one set of parameter



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PROBABILISTIC ANALYSIS



Probability distribution of tunnel squeezing (plastic deformation)

PROBABILISTIC ANALYSIS





Cumulative distribution of actually measured and predicted tunnel strains

PROBABILISTIC ANALYSIS

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Advantage

- Take care on the variation in the parameters
- Stress conditions depends on the type of methods used
- Strong tool to address deformation uncertainty

<u>Disadvantage</u>

- Dependent on the calculation method used
- Interpretational skill and experience

SUMMARY

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- Plastic deformation (tunnel squeezing) is a serious instability problem that needs to be address carefully.
- Methods that address in-situ stress state, rock mass quality parameters are the one that should be used in assessing the tunnel deformation.
- Both analytical, numerical and probabilistic approaches are useful tool to estimate plastic deformation.
- Remember, selection of the methodology is the key here for the success.