



Vågåmo flomtunnel



Inntak



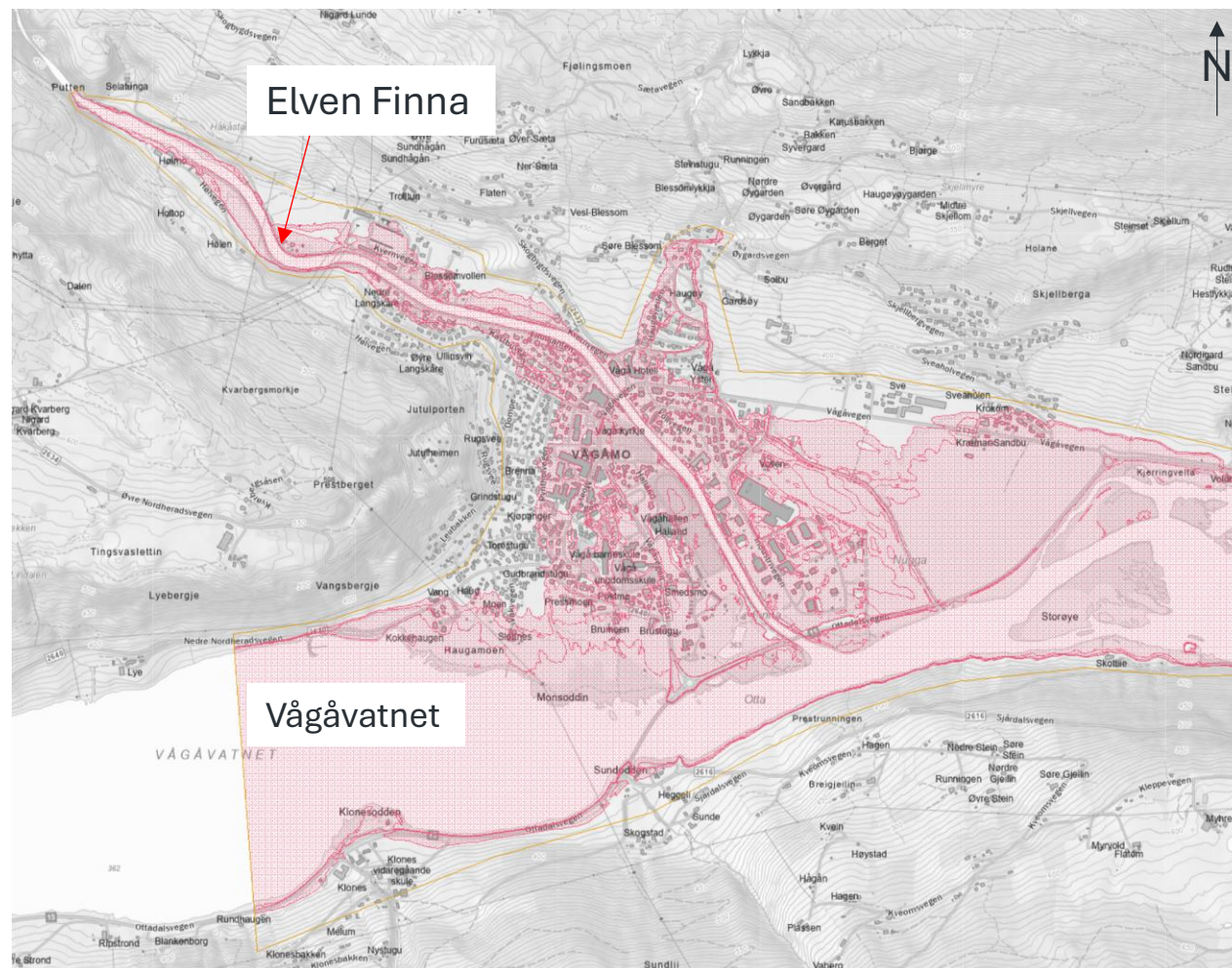
Utløp

Tidligfaseplanlegging i sterkt forvitret berg

Marie Foldøy Solem og Gaute Moe Fløan
Vårsleppet 12.03.2026



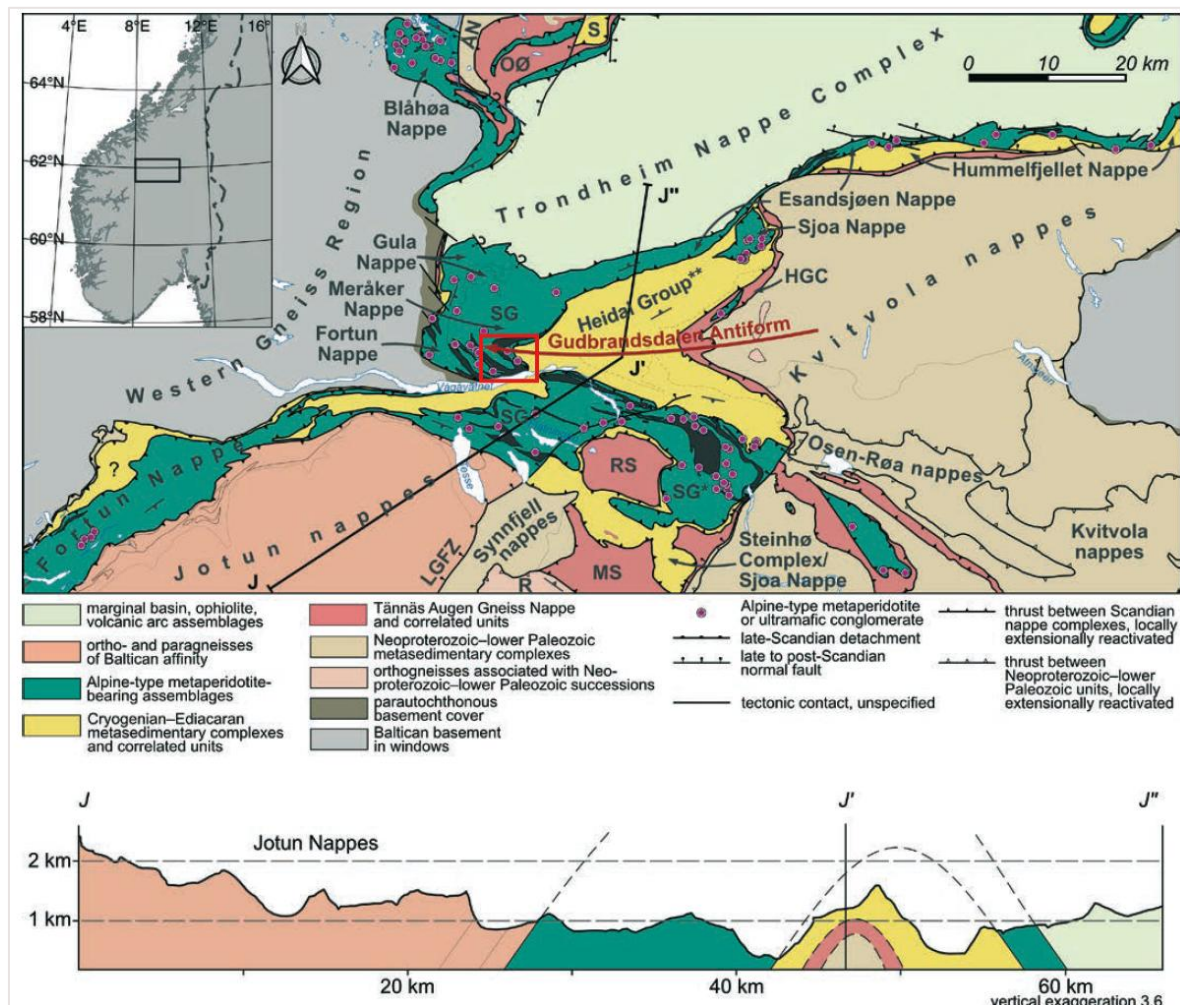
Bakgrunn



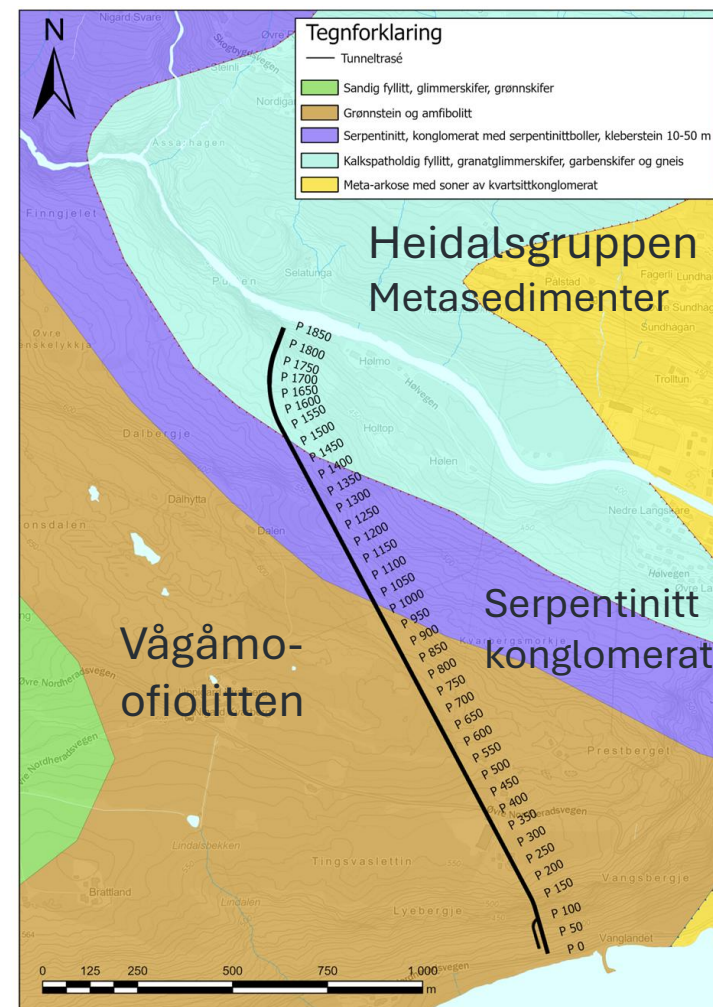
Flomsoner fra NVE Atlas.



Grunnforhold



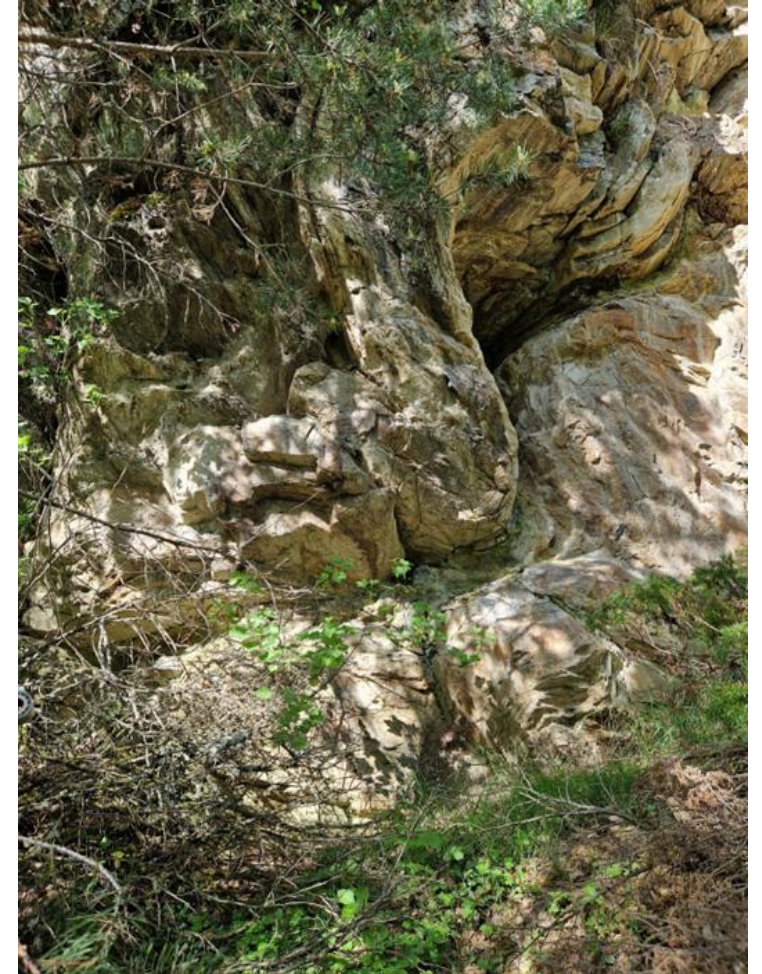
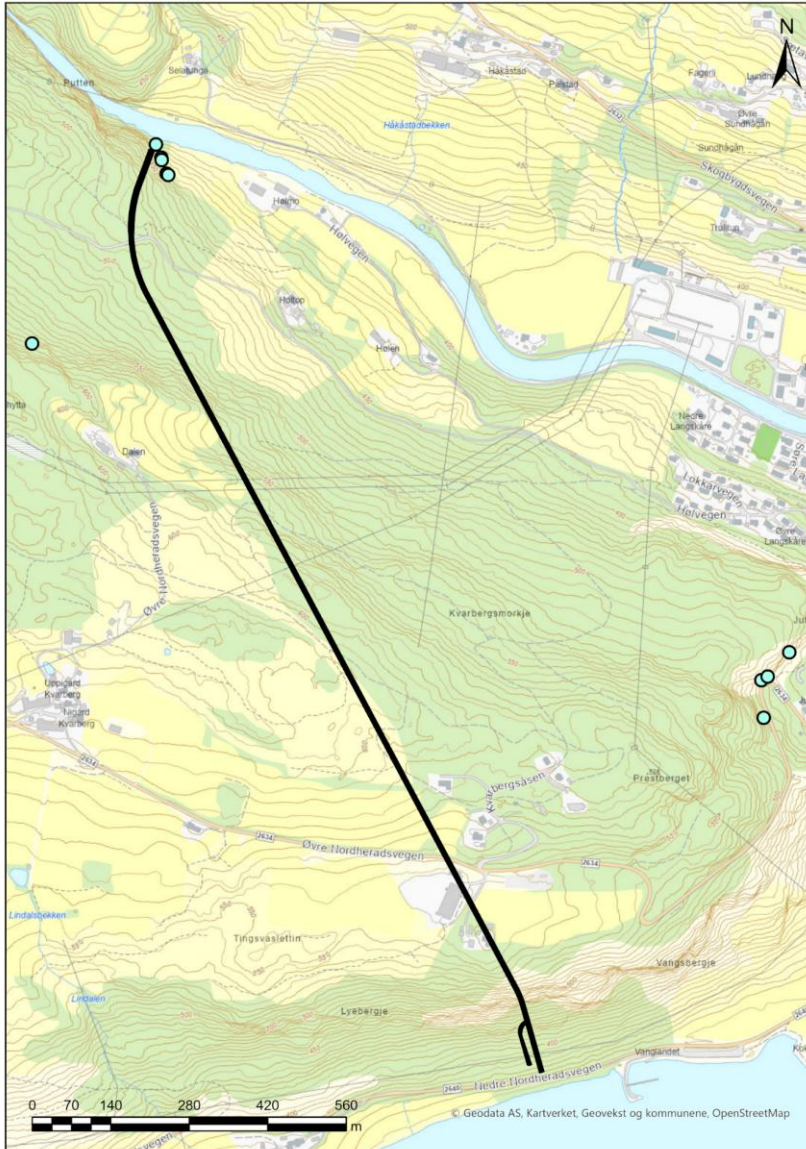
Geologisk kart fra den nordlige delen av Gudbrandsdalen.
Hentet fra Jakob et. al. 2022.



NGU: 1:250 000 berggrunnskart



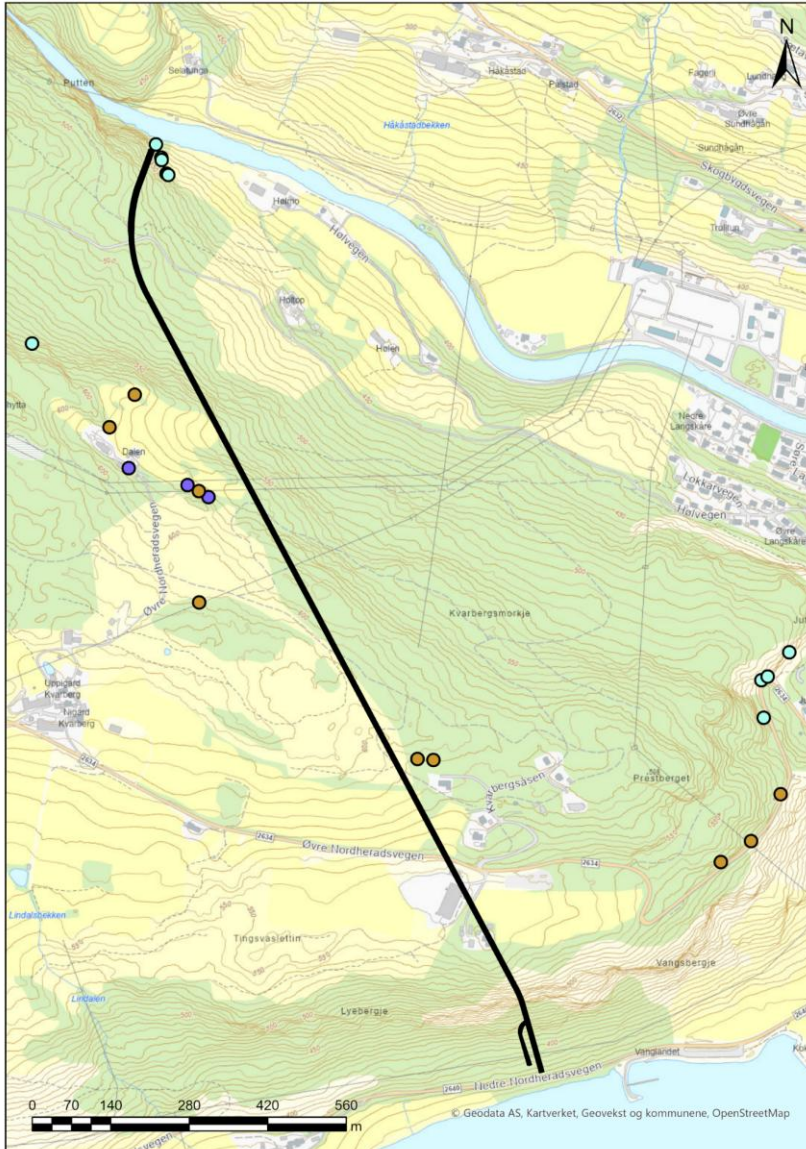
Grunnforhold



Metasedimentære bergarter



Grunnforhold



Konglomerat med boller av serpentinit

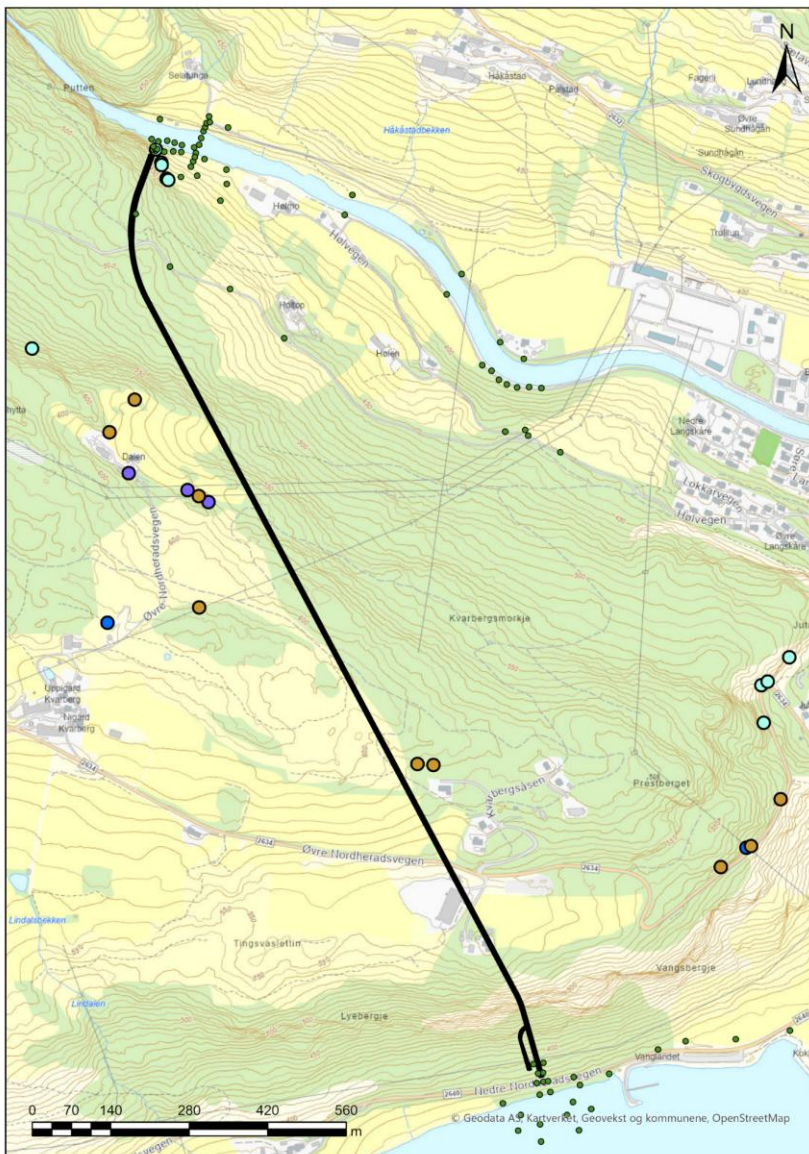


Multiconsult



Grunnforhold

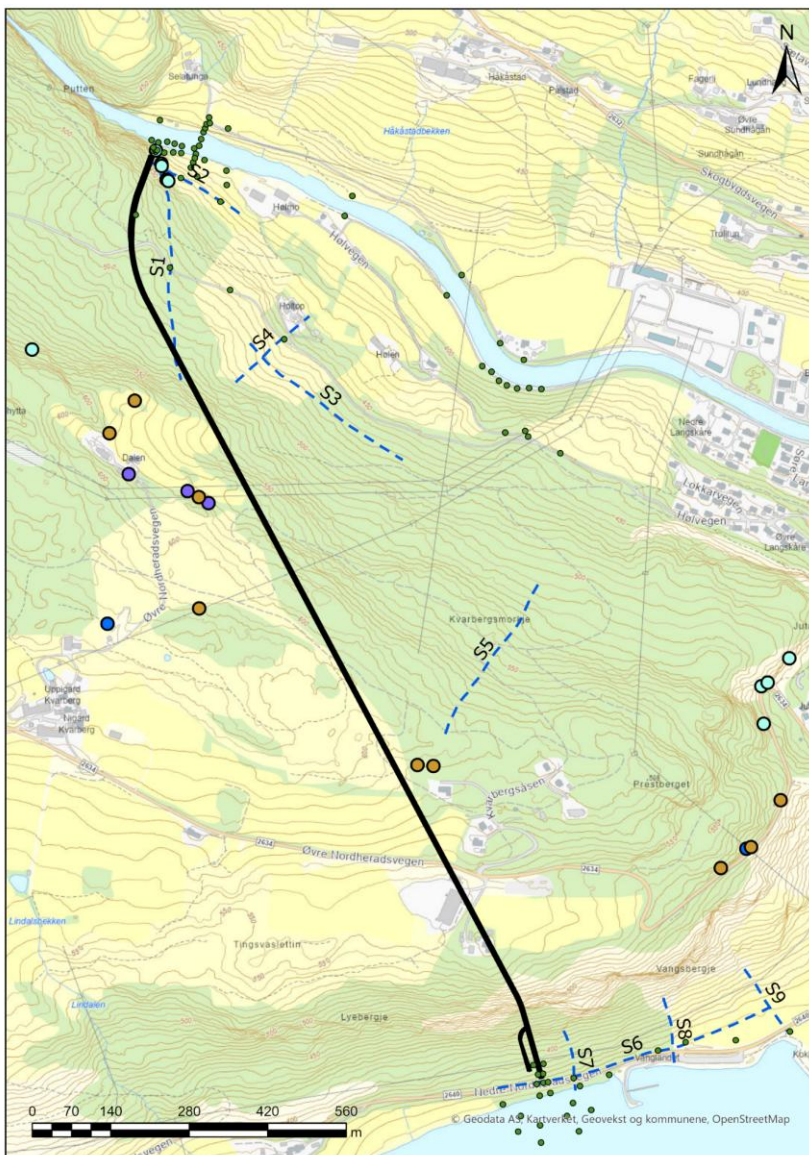
- Totalsonderinger





Grunnforhold

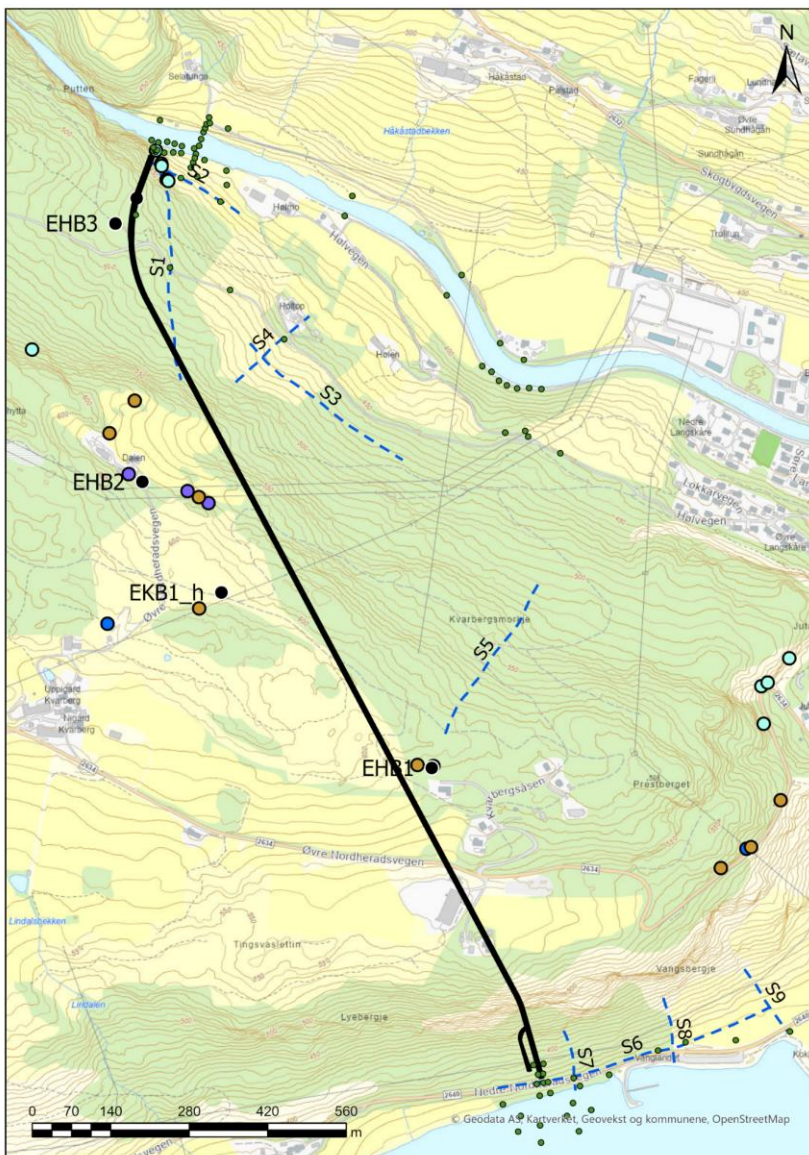
- Totalsonderinger
- Seismikk





Grunnforhold

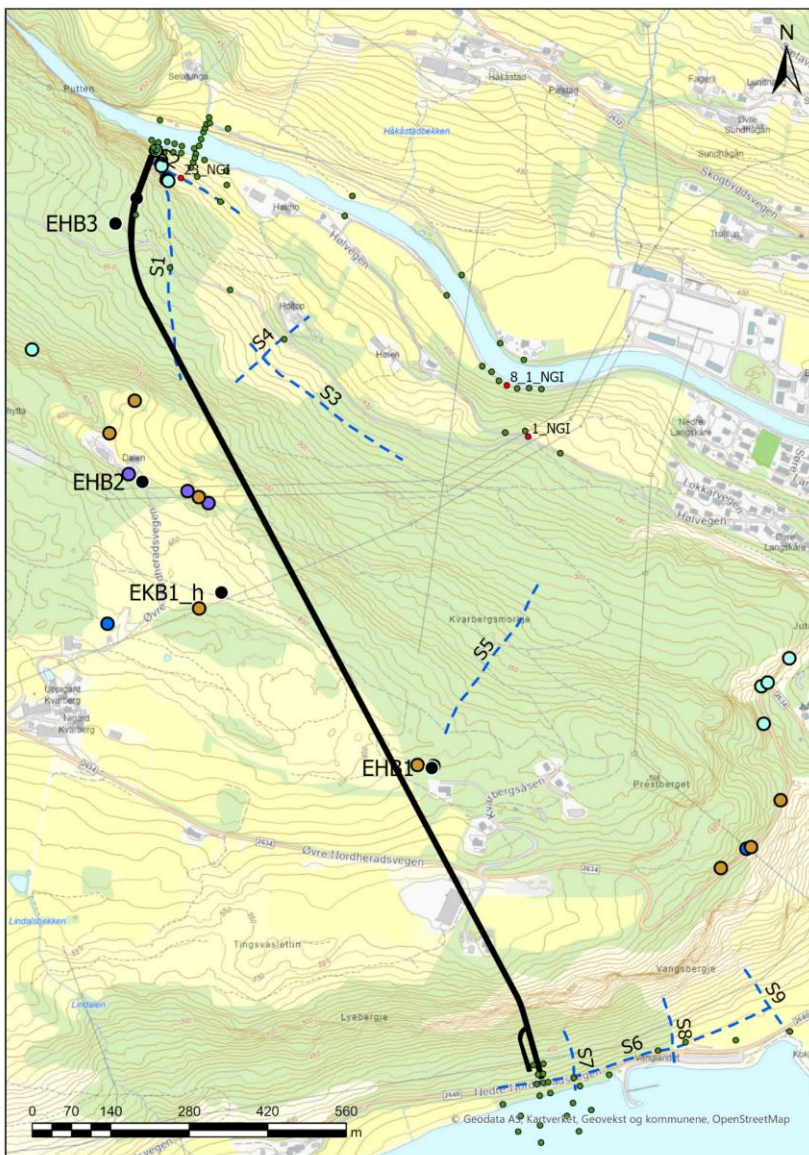
- Totalsonderinger
- Seismikk
- Hammerboringer





Grunnforhold

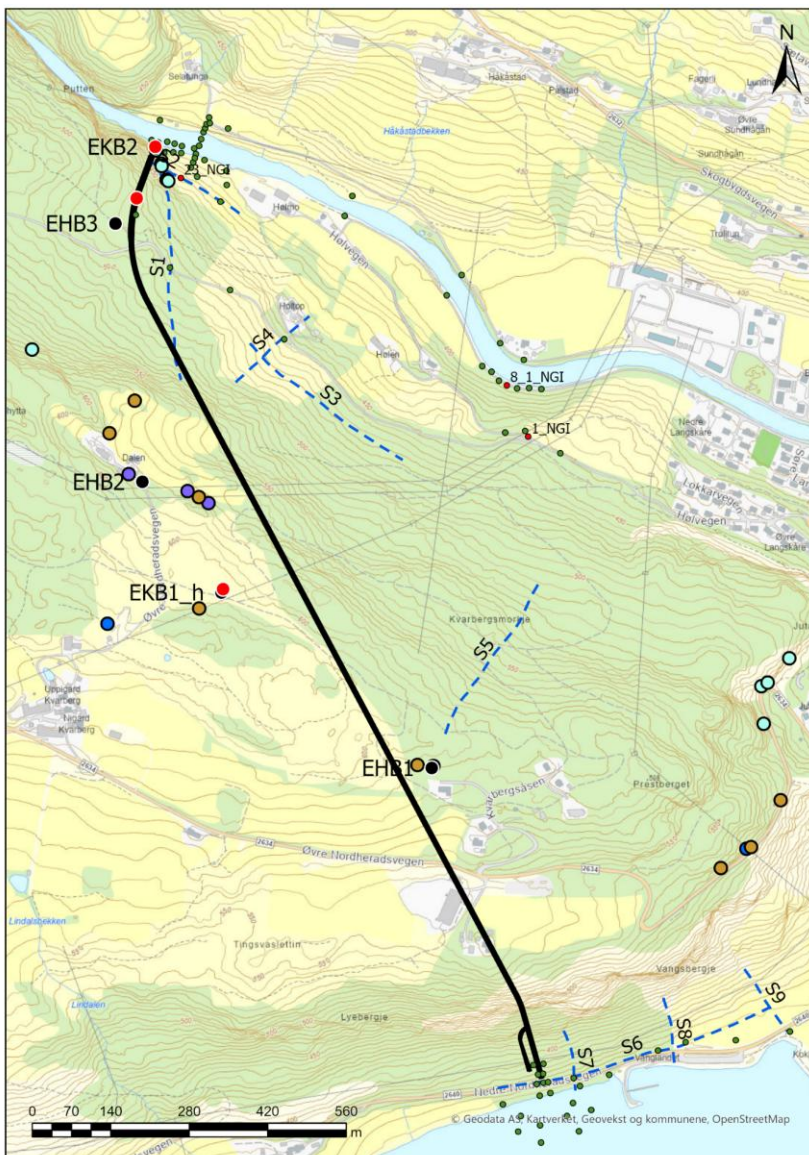
- Totalsonderinger
- Seismikk
- Hammerboringer
- Korte kjerneboringer





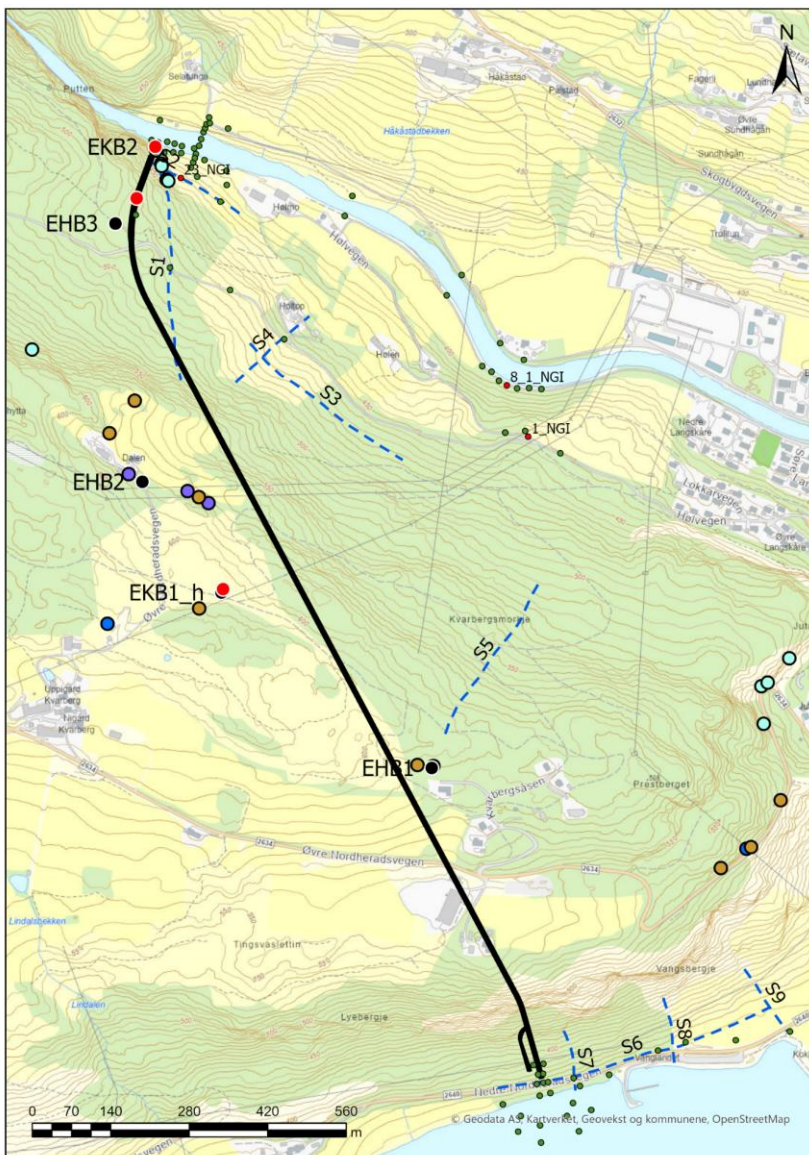
Grunnforhold

- Totalsonderinger
- Seismikk
- Hammerboringer
- Korte kjerneboringer
- Lange kjerneboringer





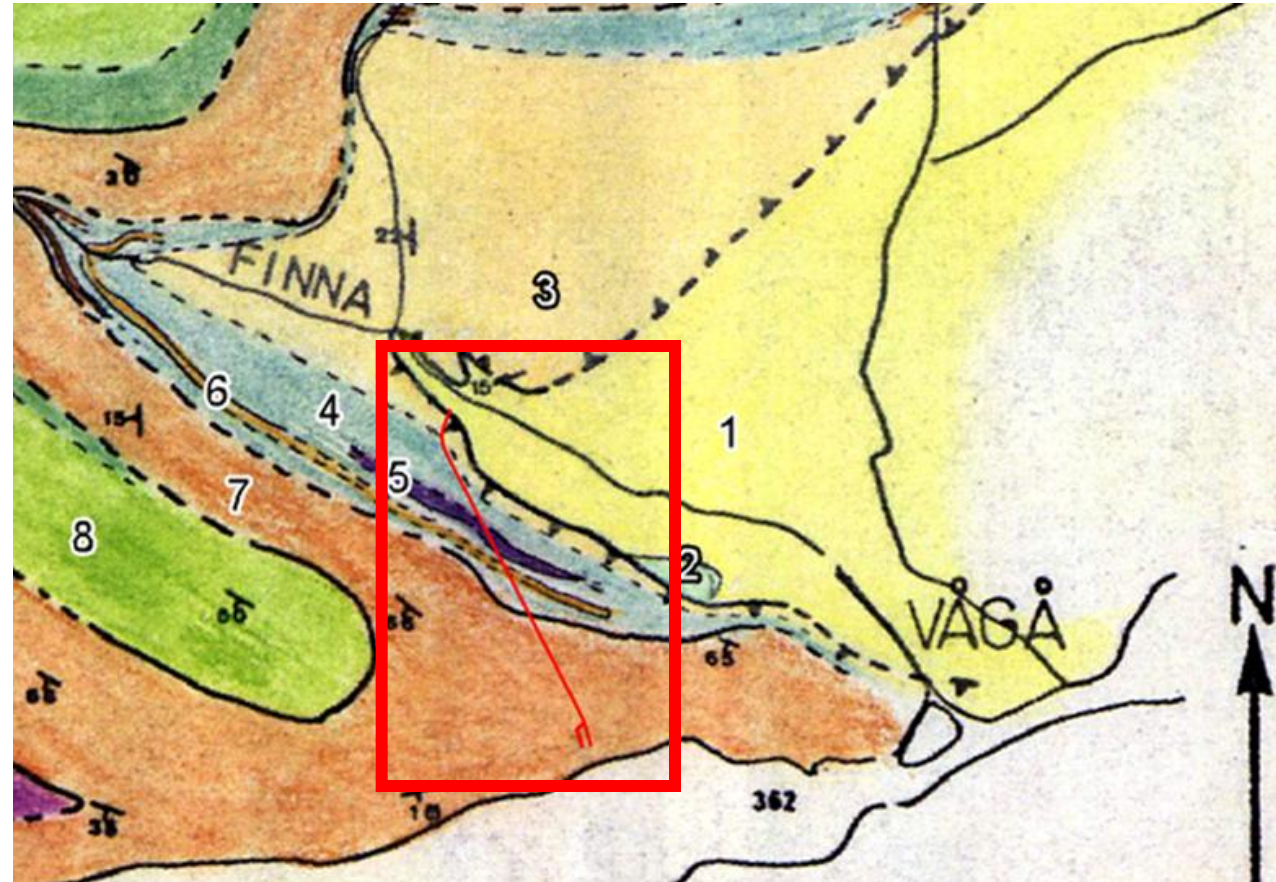
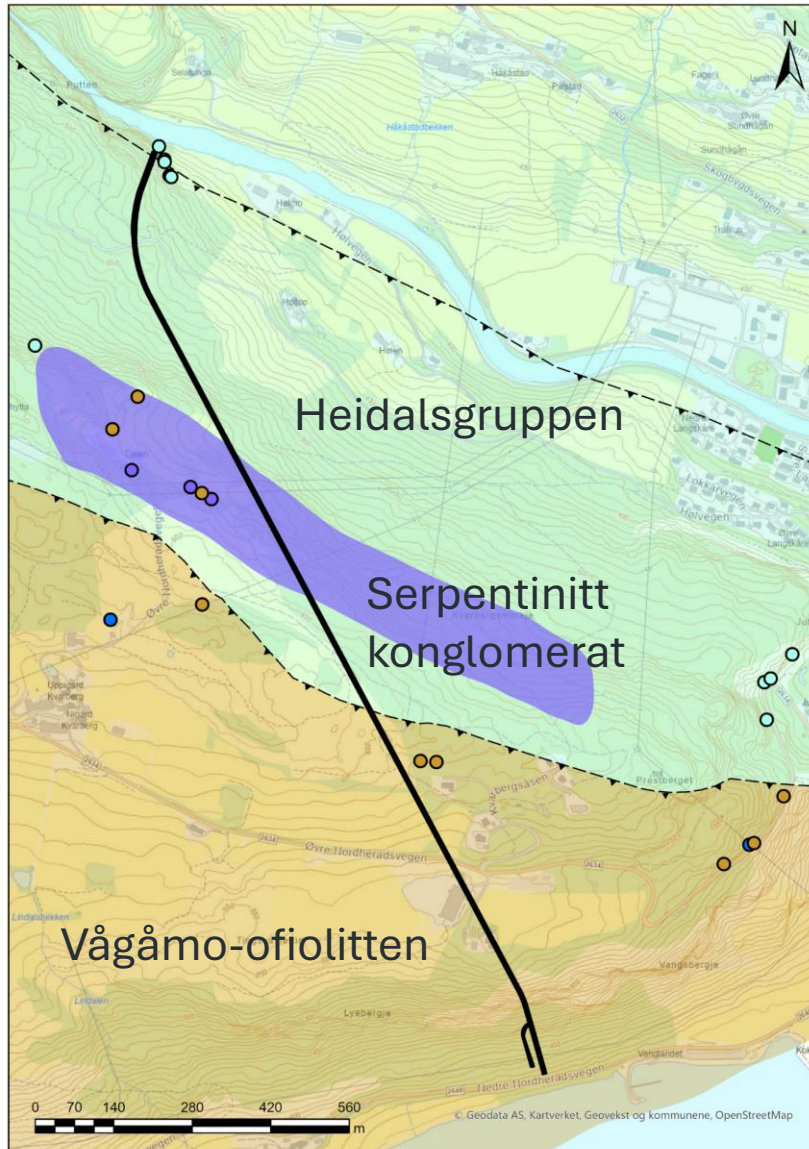
Grunnforhold



- Totalsonderinger
- Seismikk
- Hammerboringer
- Korte kjerneboringer
- Lange kjerneboringer
- Bergmekaniske og geokjemiske labundersøkelser



Grunnforhold

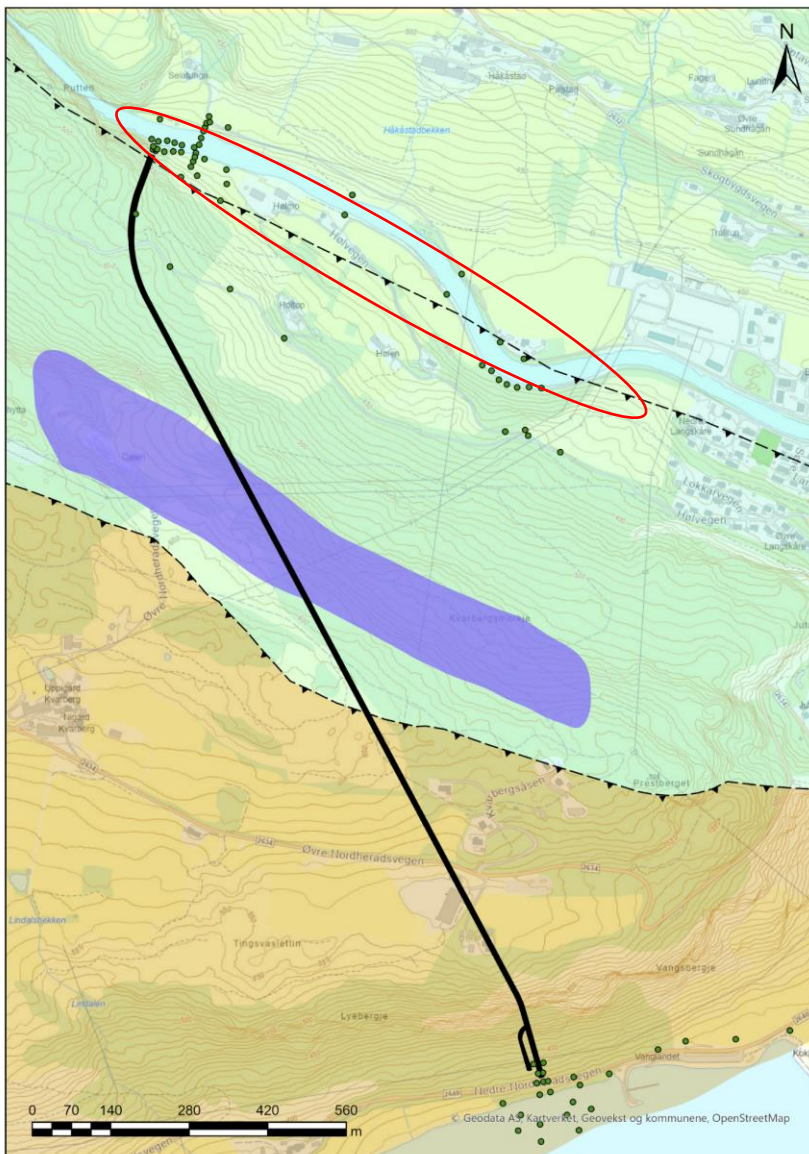


Manuskart 1:50 000 over Vågå fra 1976. Kartlagt av Edvard Iversen for NGU.



Grunnforhold

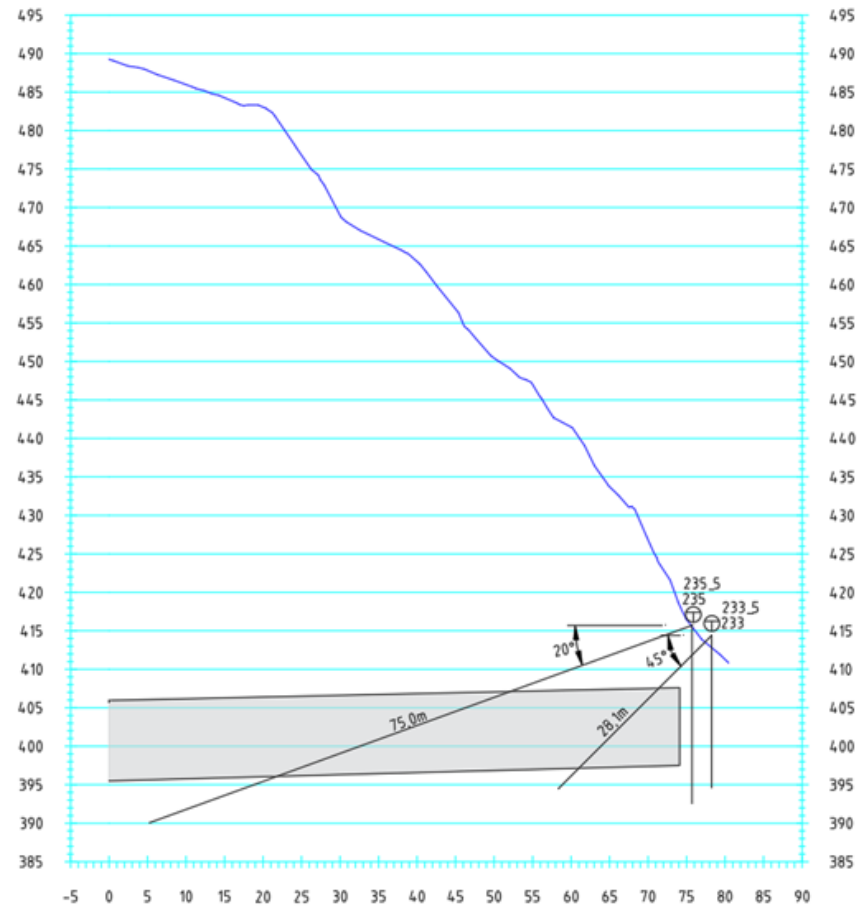
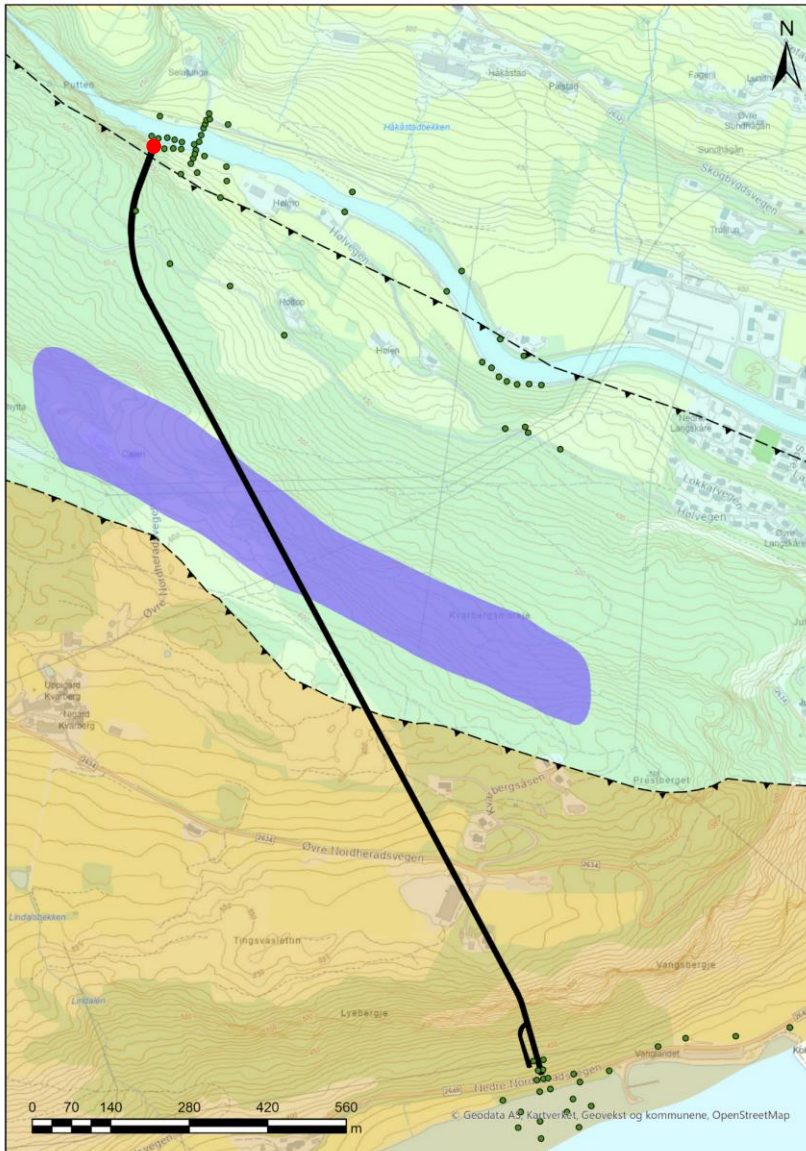
- Totalsonderinger:
Vanskelig å skille mellom løsmasser og berg!





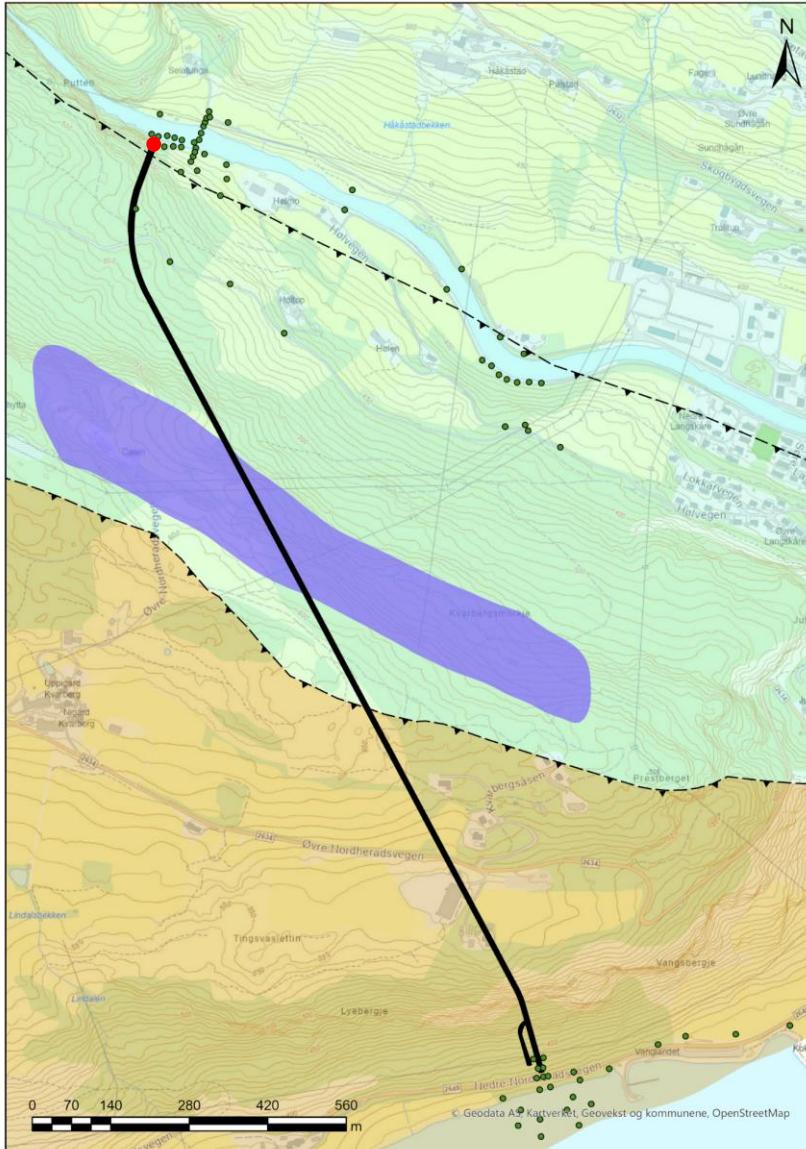
Grunnforhold

- Totalsonderinger:

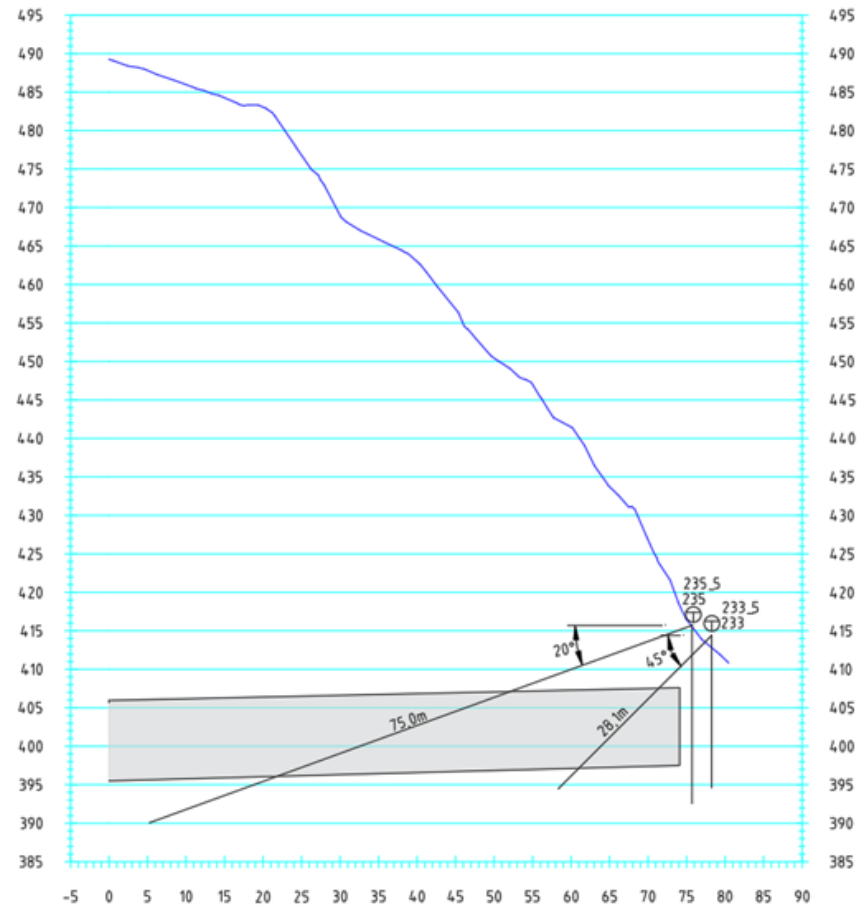




Grunnforhold



- Totalsonderinger:





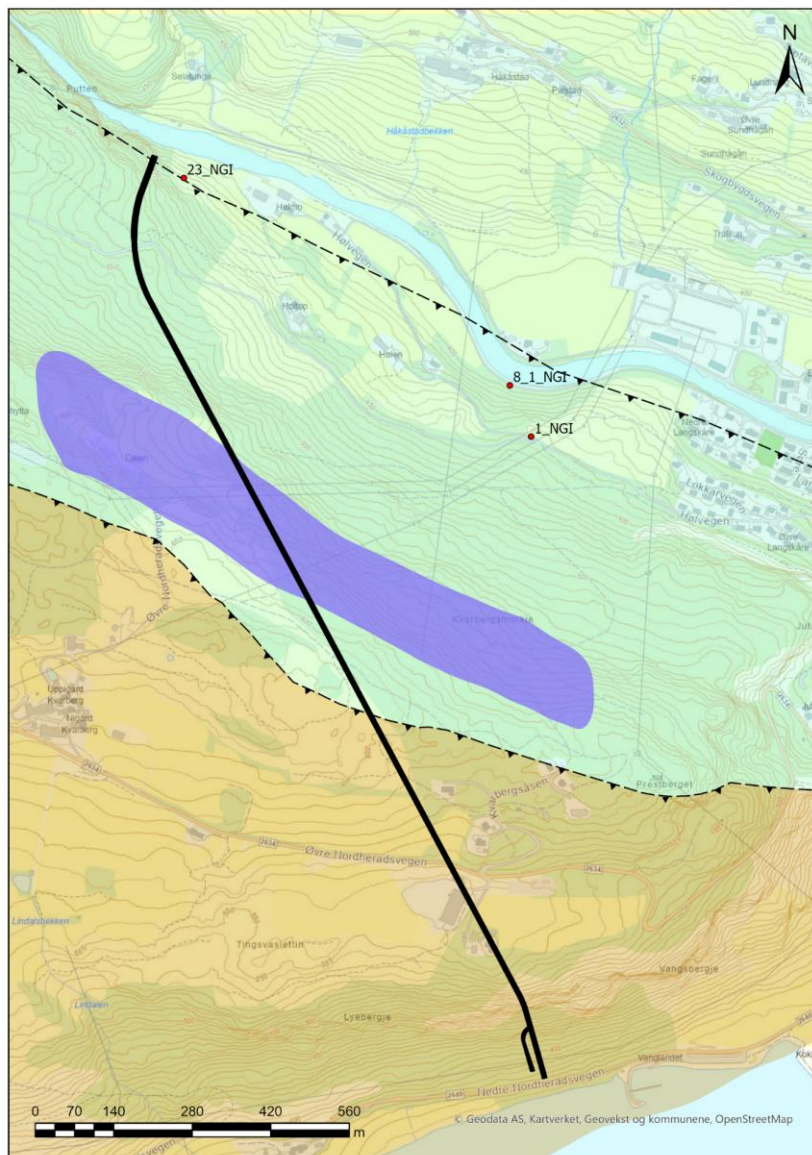
Grunnforhold

- Korte kjerneboringer:

K3: 18,07 - 23,27 m



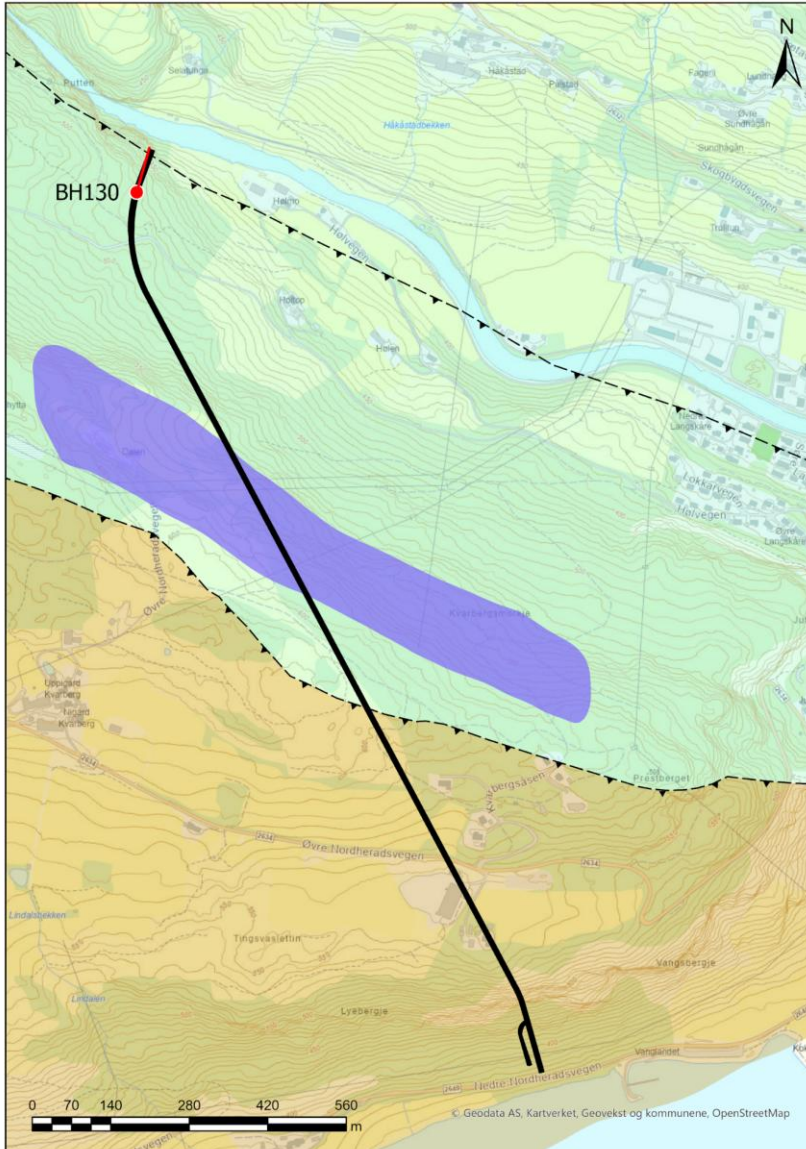
K4: 23,27 - 29,85 m





Grunnforhold

- Kjerneboring BH130



K11: 26,35 – 29,35 m

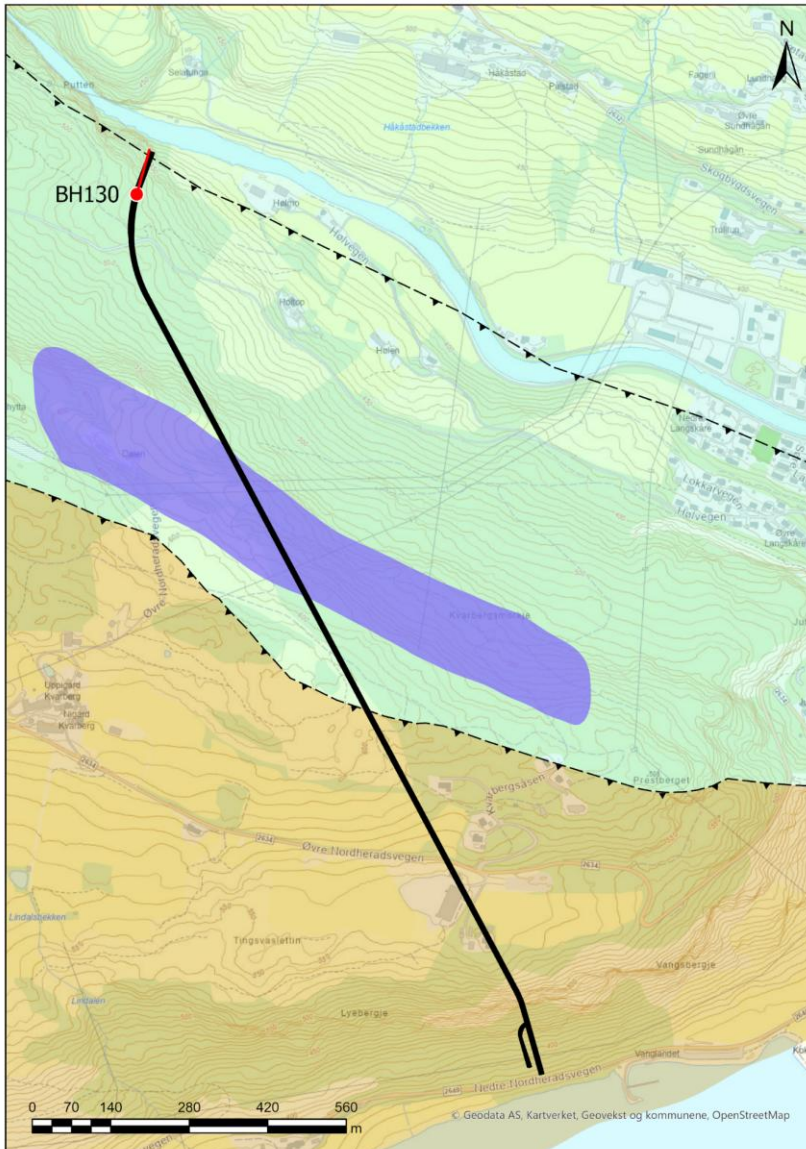


0 - 47 m: Kjerneboring

47 – 116 m: Hammerboring grunnet dårlig berg

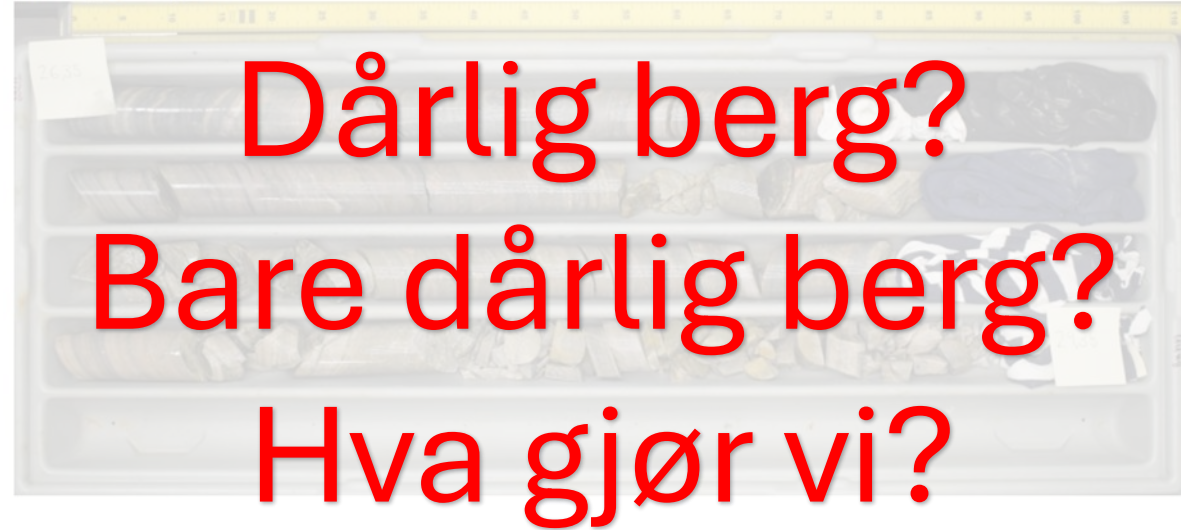


Grunnforhold



- Kjerneboring BH130

K11: 26,35 – 29,35 m

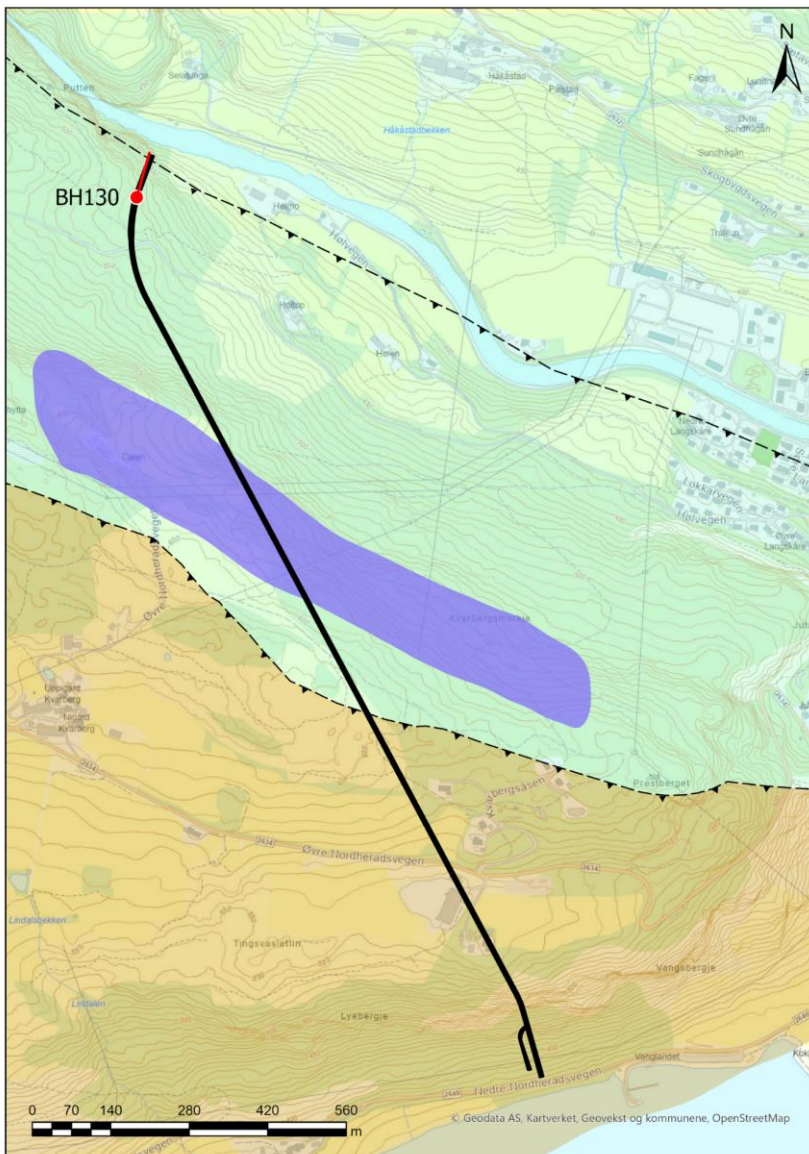


0 - 47 m: Kjerneboring

47 – 116 m: Hammerboring



Grunnforhold



- Kjerneboring BH130

K11: 26,35 – 29,35 m



Jo!
Vi tar en kjerneboring
til!

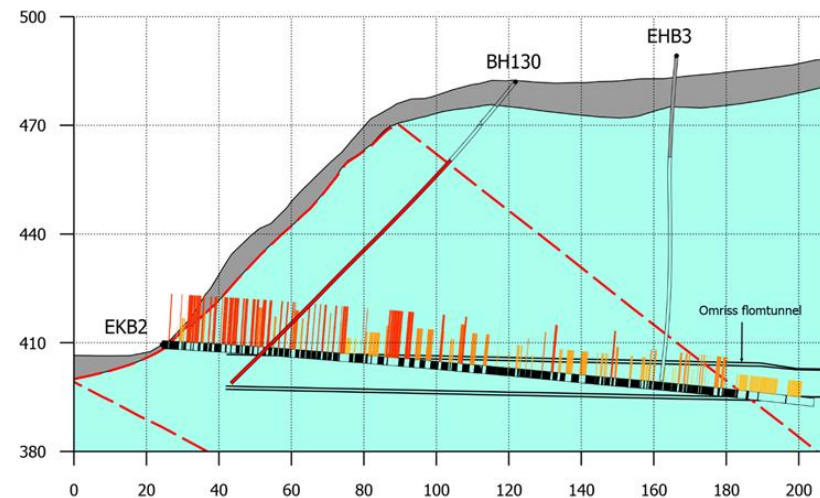
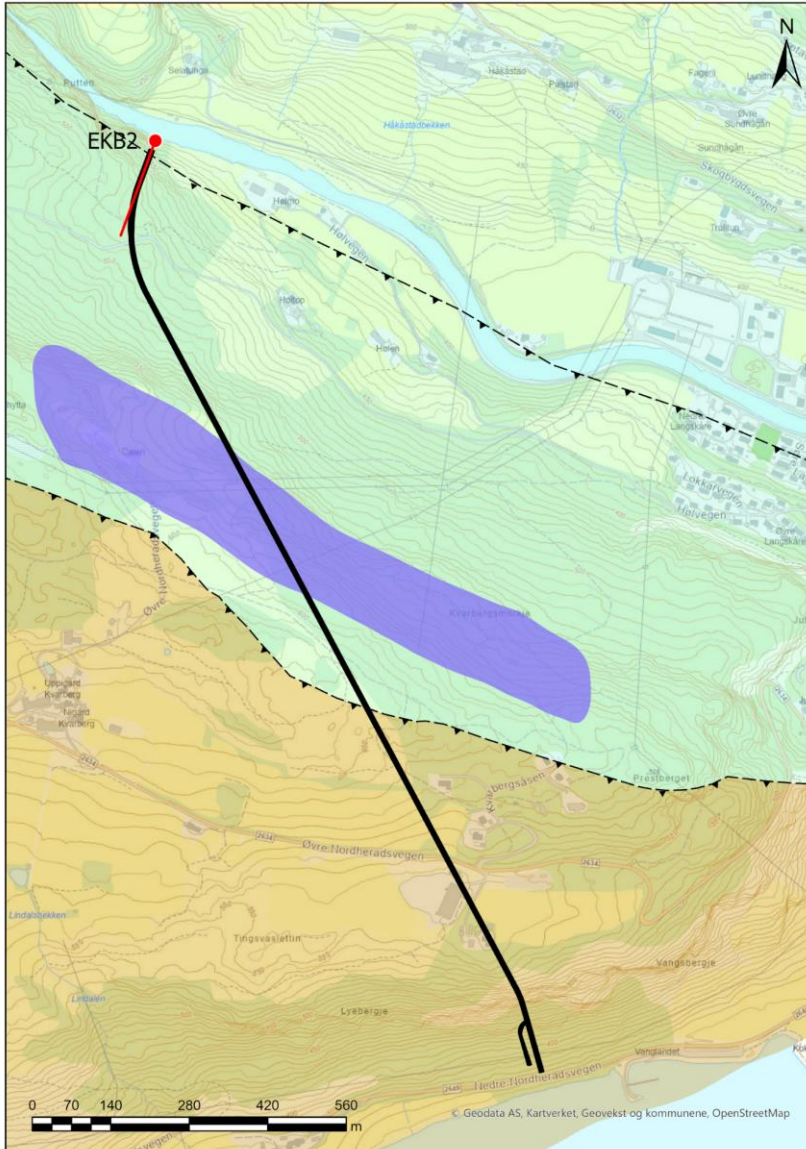
0 - 47 m: Kjerneboring

47 – 116 m: Hammerboring



Grunnforhold

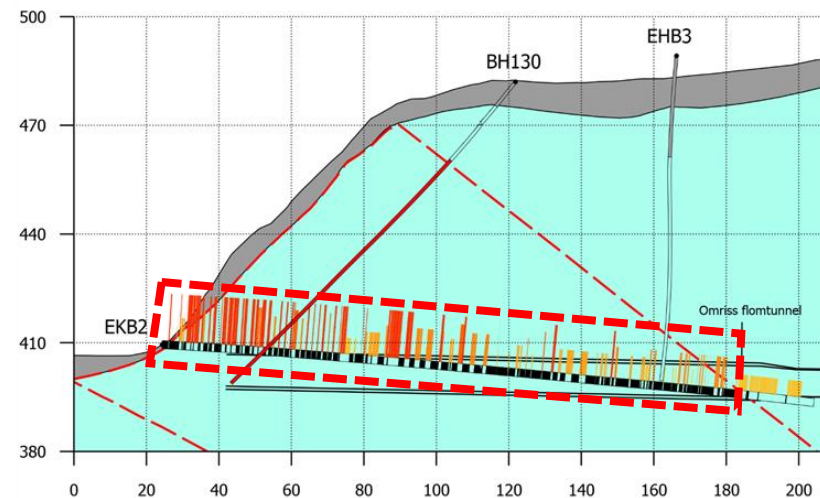
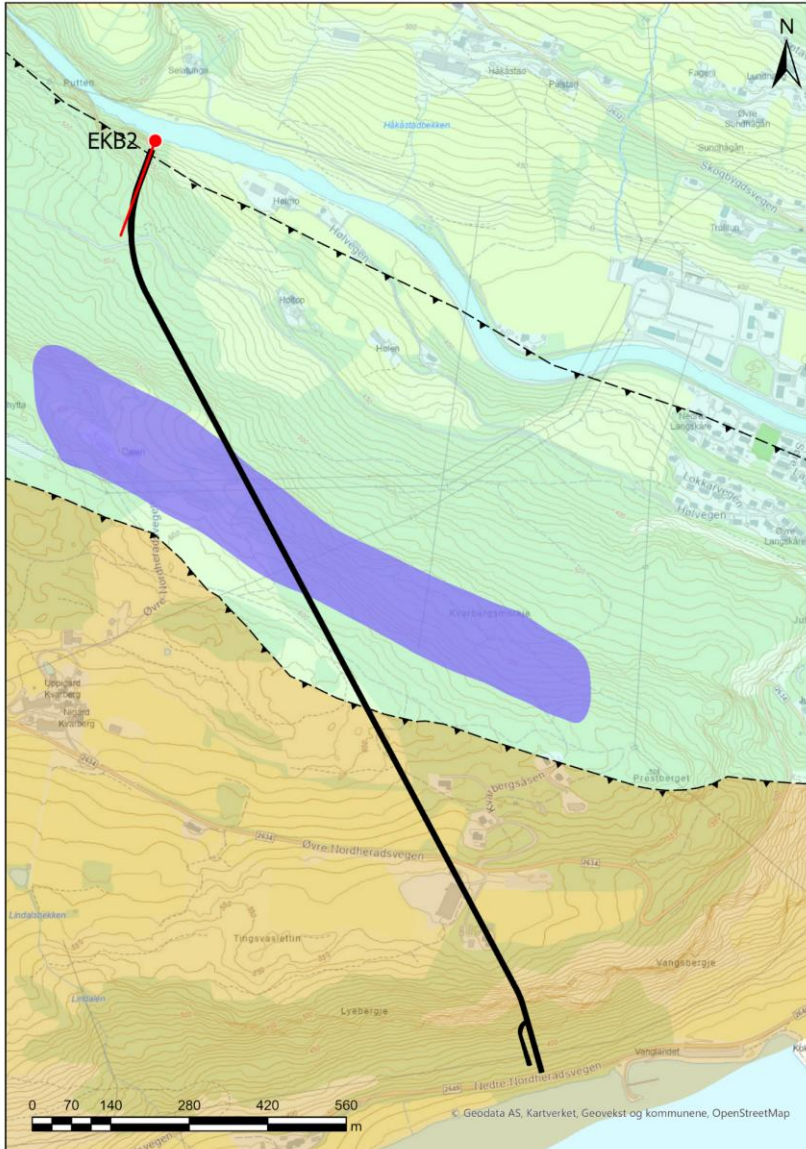
- Kjerneboring EKB2 – Tribble tube core





Grunnforhold

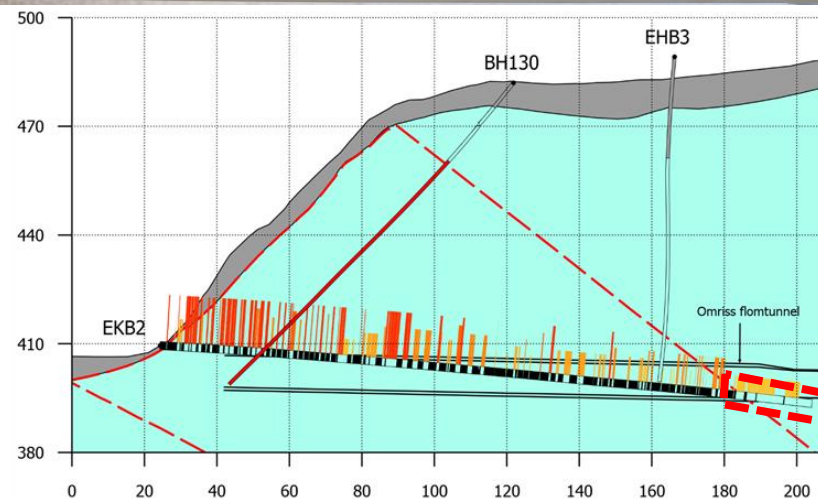
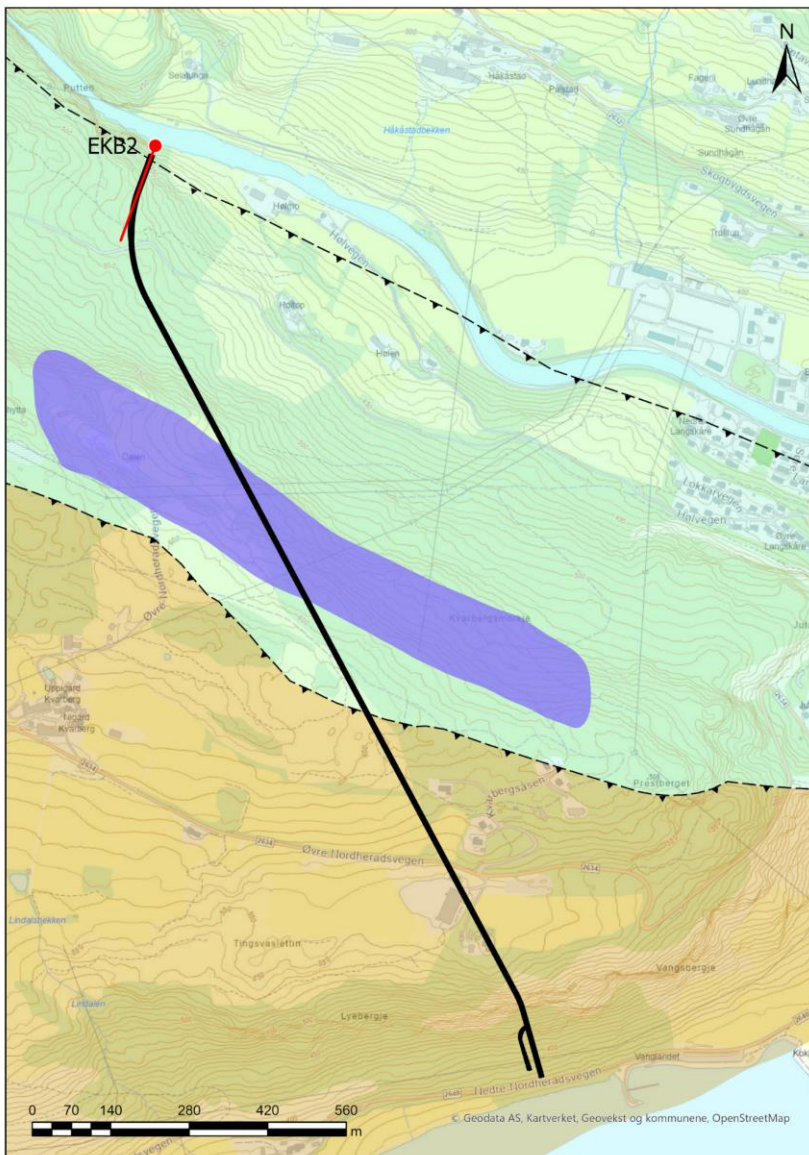
- Kjerneboring EKB2 – Tribble tube core





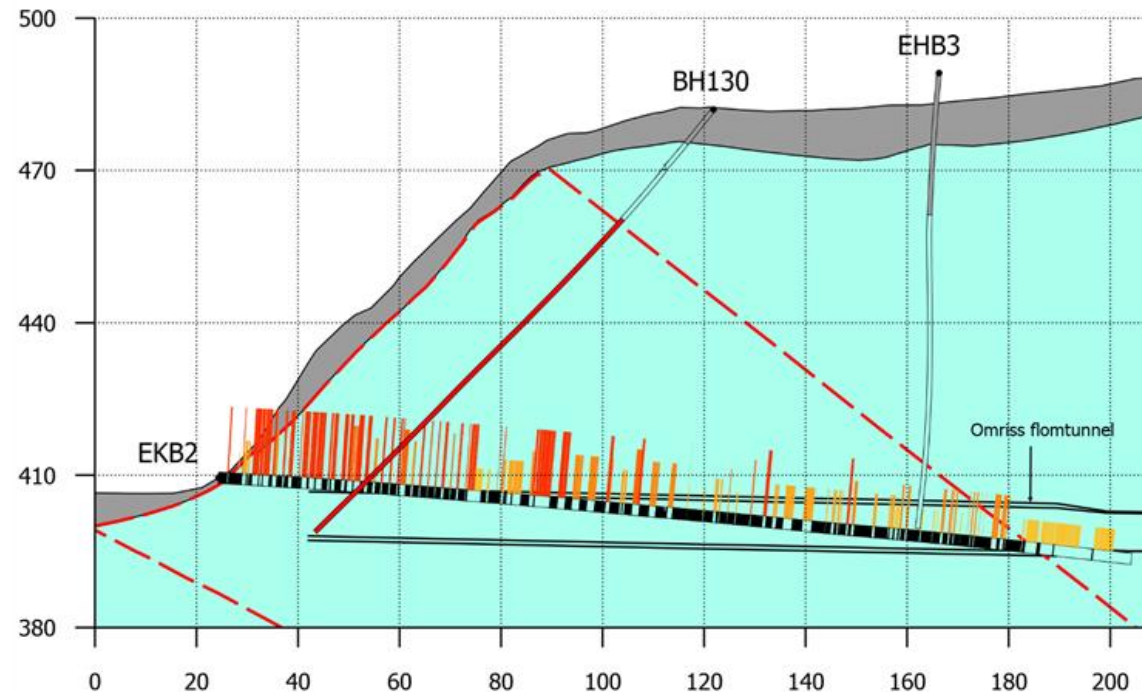
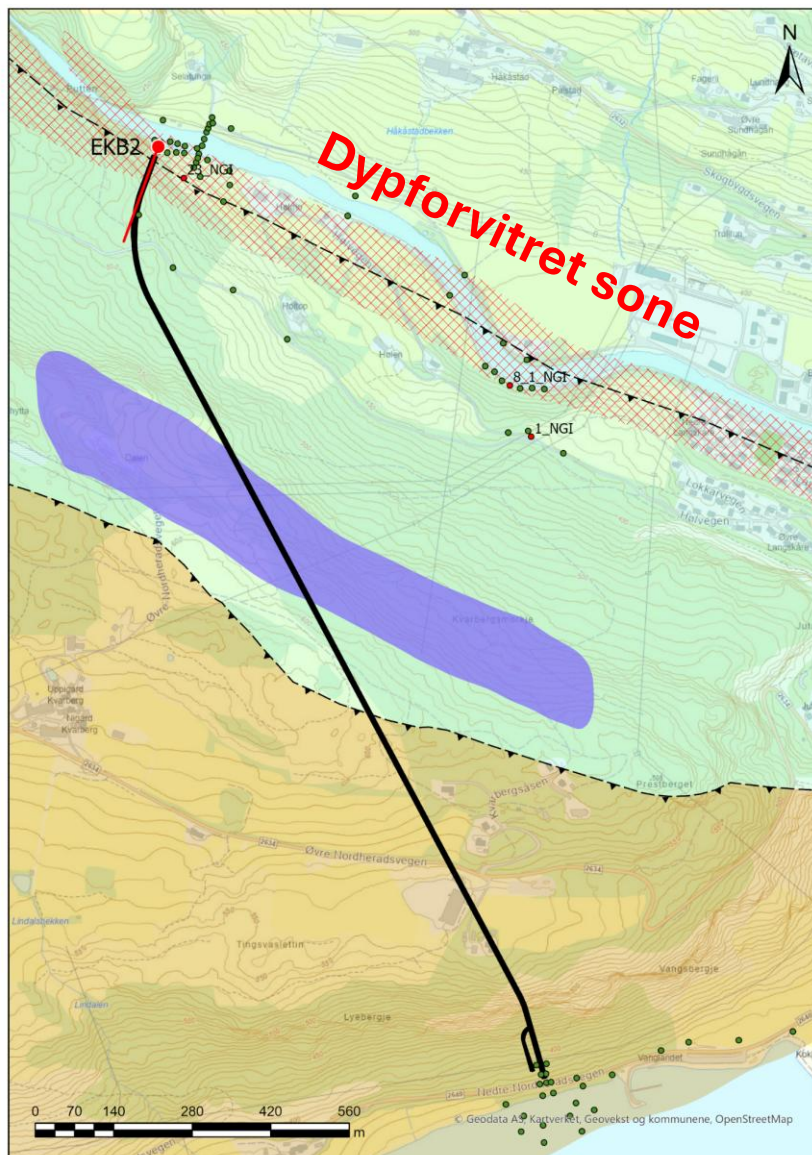
Grunnforhold

- Kjerneboring EKB2 – Tribble tube core





Grunnforhold



Tegnforklaring

Forvitring i EKB2

0 0.8 1.5 2.2 3



Heidalsgruppen

Løsmasser

Sterkt forvitret berg i BH130

Kjernetap i EKB2

Tolket grense for sterkt forvitret berg



Målestokk: 1:1,300

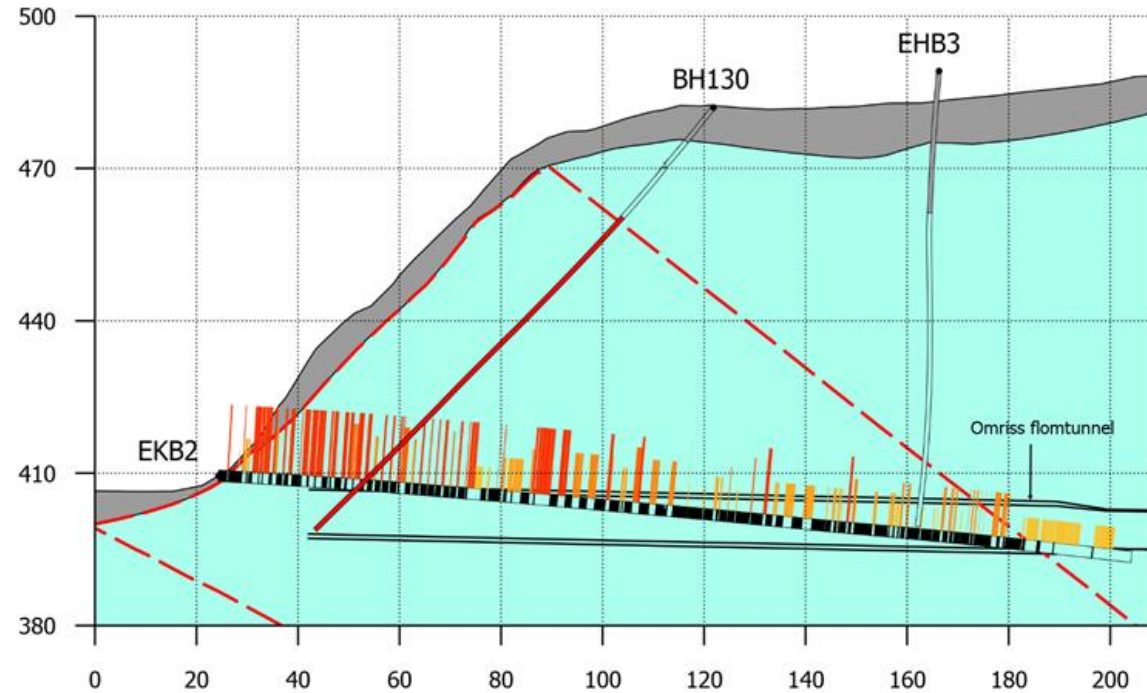
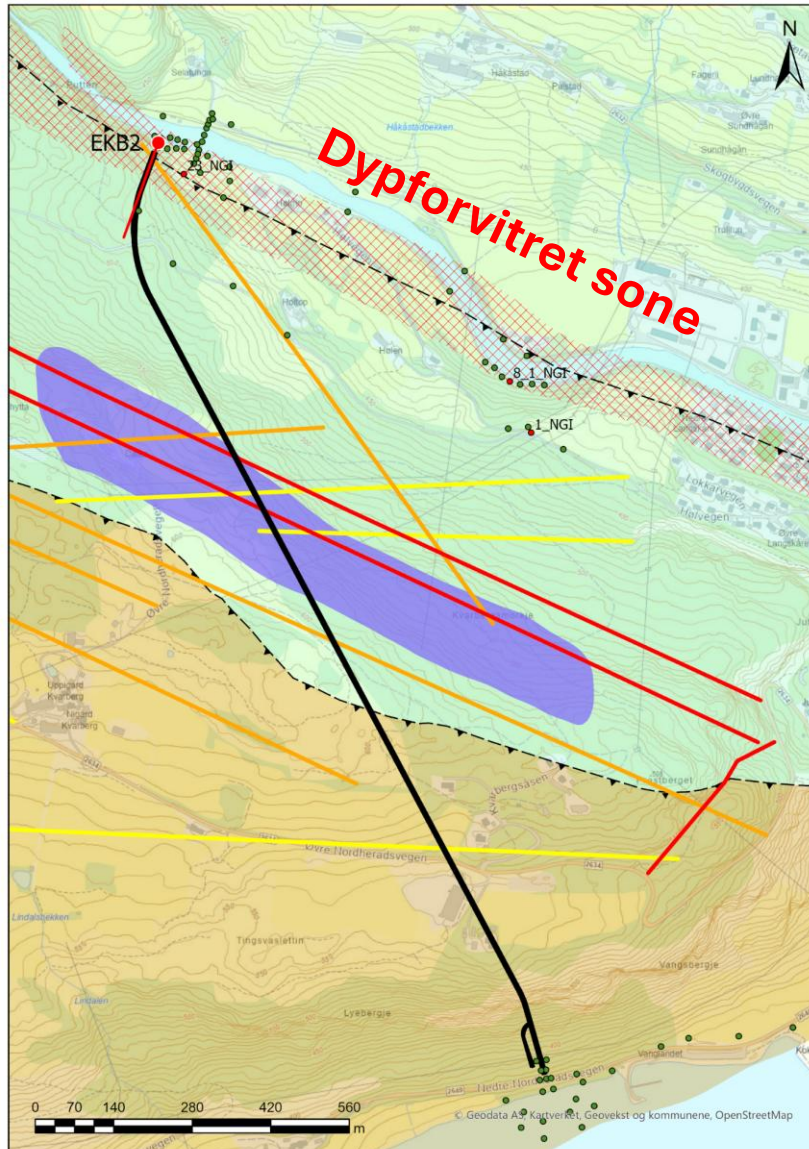
Vertikal forsterkning: 1x

0m 50m





Grunnforhold



Tegnforklaring

Forvitring i EKB2

0 0.8 1.5 2.2 3



Heidalsgruppen

Løsmasser

Sterkt forvitret berg i BH130

Kjernetap i EKB2

Tolket grense for sterkt forvitret berg



Målestokk: 1:1,300

Vertikal forsterkning: 1x

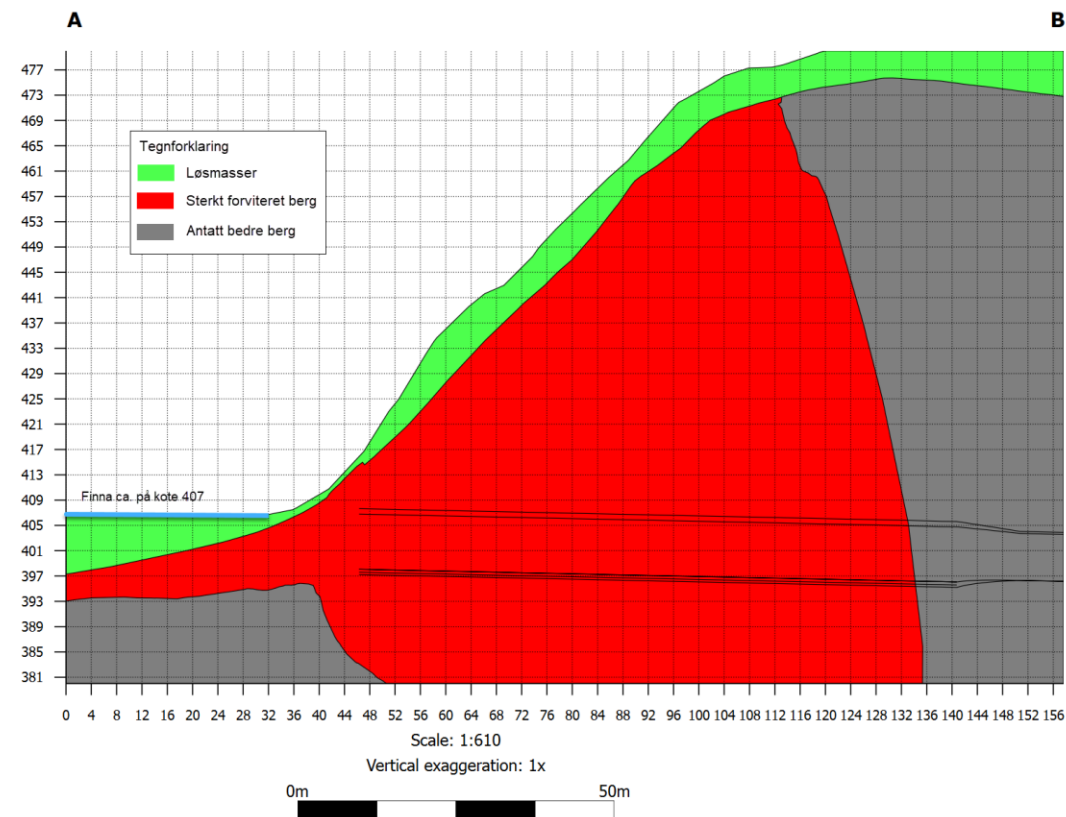
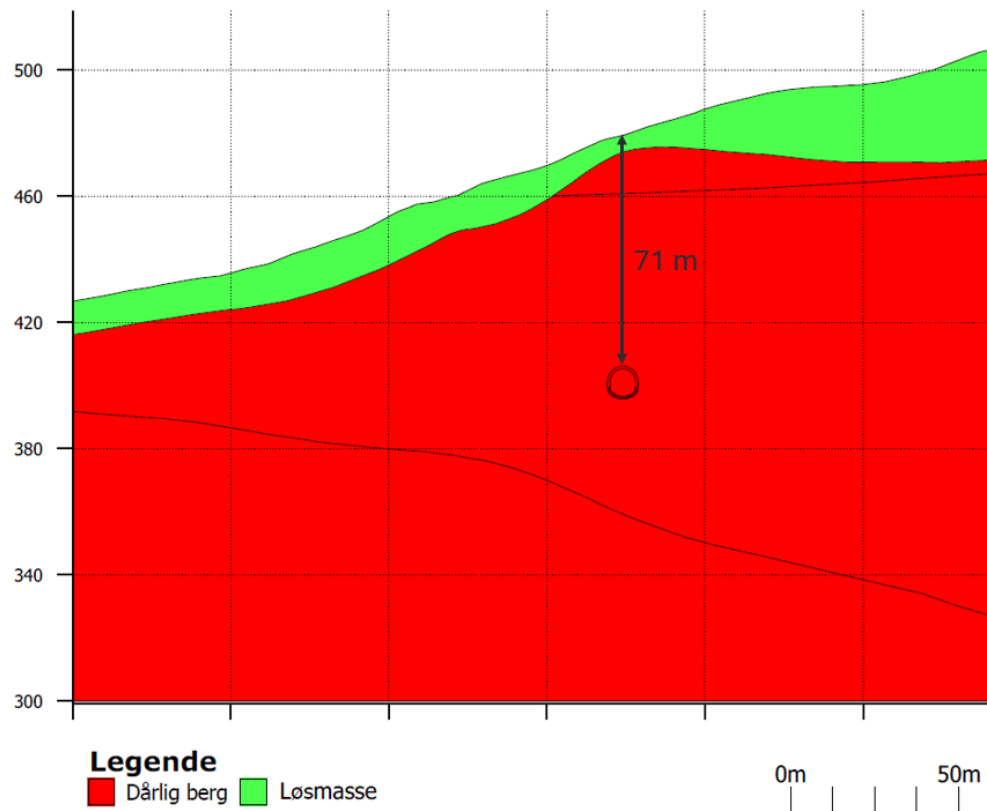




Stabilitetsberegning i RS2

Formål og begrensninger

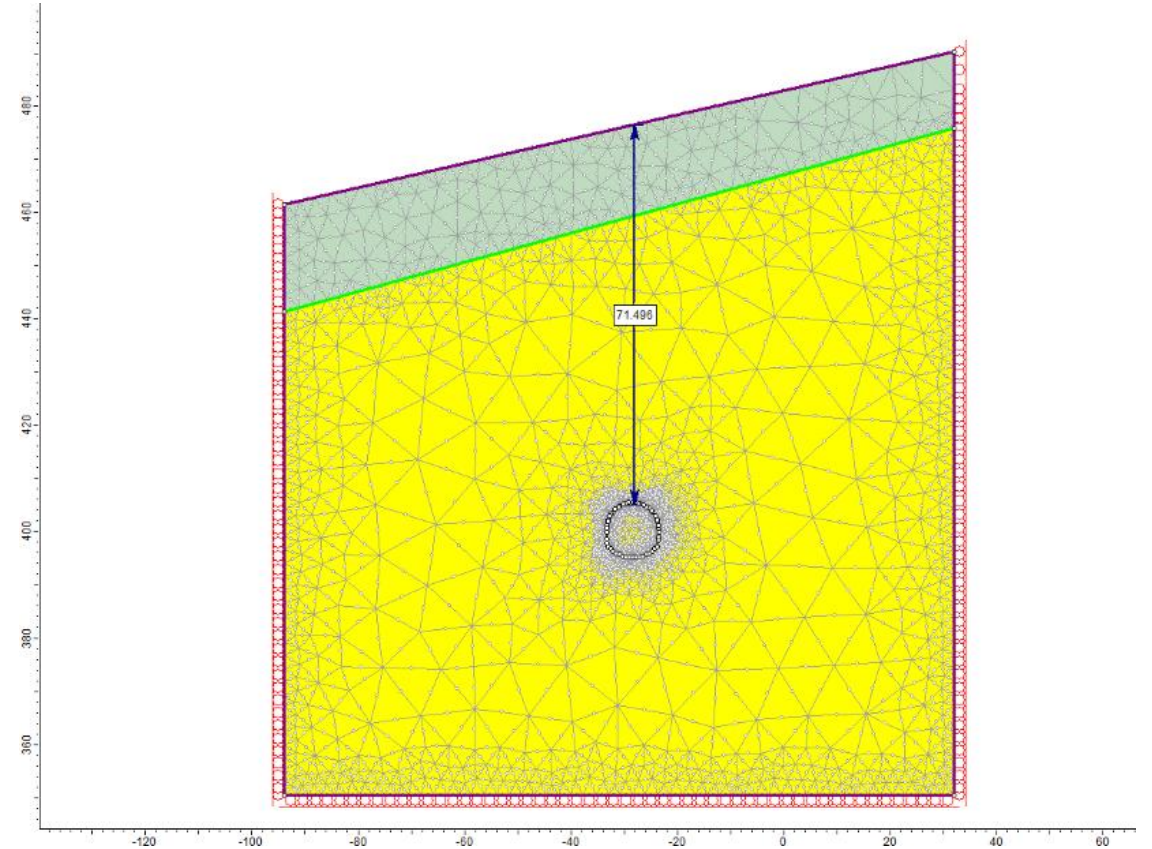
- Formål: Hvilke tiltak må til for å drive tunnel i den sterkt forvitrede sonen?
- Begrensninger: Tilgang på representativ data





Modelloppsett

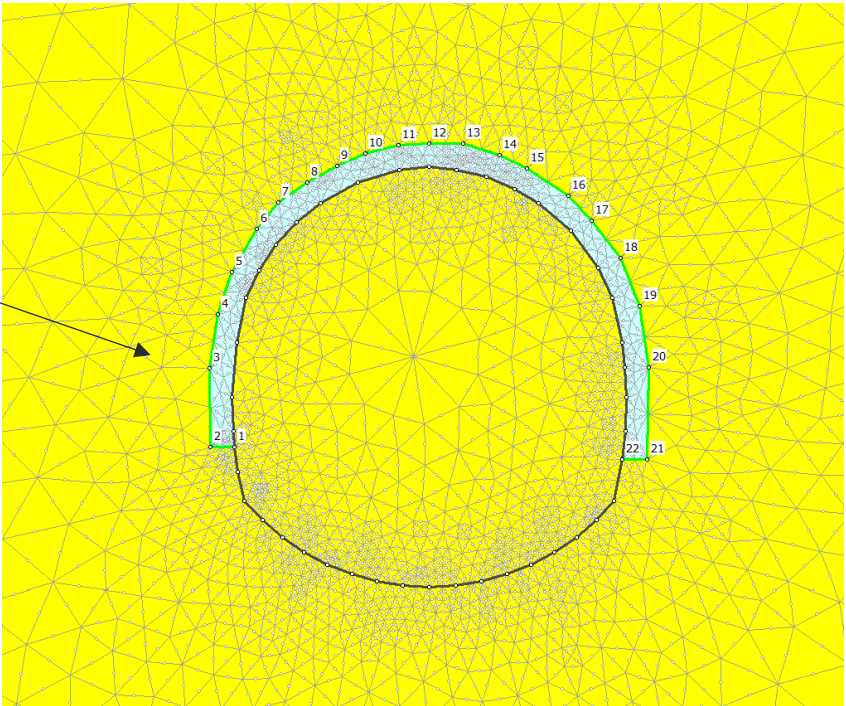
- Klassisk 2D FEM modell, RS2
- Kritisk snitt
- Generalisert Hoek brown (GSI-metode)
- Metode for skring bak stuff for å simulere 3D-effekter





Modelstrategi

Nr	Tilstand	Beskrivelse
1.	In situ	In-situ tilstand uten berguttak
2.	Berguttak	Fullprofil uttak av flomtunnel uten bergsikring (3)
3.	Forsterkning	fullprofil berguttak med forsterket rørskjermlag (4 m bak stuff) (1,2)
4.	Permanent bergsikring	Analyse av bergsikringsdesign (3,4)
5.	Laster fra driftsfase.	Flomtilstand
6.	Sensitivitetsanalyser	Grunnvann, bergmasseparametre (GSI)



Kilder

1. Hoek, Evert. *Numerical Modelling for Shallow Tunnels in Weak Rock*. Upubliserte notater.
2. Hoek, Evert. 1998. *Tunnel Support in Weak Rock*.
3. Rocscience. *Tunnel Lining Design*.
4. Terron-Almenara et.al (2024). *Permanent tunnel support with reinforced shotcrete arches and forepoling in over-consolidated till and weathered rock. A case study based on the construction of the Bergås tunnel, Norway*



Inngangsparametere

Gode inngangsparametere er en forutsetning

- Bergmasseparametere: UCS, GSI
- In situ spenninger $K=1$
- Elastisk bergsikring
- Grunnvann ved planlagt tunnelheng kote 414

GSI $\approx$ 20-30 (30-40 % av påhugg)
 σ_{ci} (dårligst) 2-3 MPa
 σ_{ci} (best) 20-25 MPa



GSI $\approx$ 25-30 (50-60 % av påhugg)
 σ_{ci} (dårligst) 2-3 MPa
 σ_{ci} (best) 20-25 MPa



GSI $\approx$ 40-45 (0-20 % av påhugg)
 σ_{ci} (dårligst) 10-25 MPa
 σ_{ci} (best) 25-50 MPa

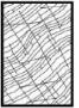


Parameter	Bergmasse ved påhugg		
	Estimat lokalt, i dårligste område	Estimat lokalt, i øvrige del av påhuggsområdet	Globale parametere
Andel av global	0.4	0.6	N/A
Bergmassestype (fra tabell om Flysch)	E	D/E	D/E
GSI	20	25	23
σ_{ci} (feltestimat, MPa)	2	25	16
σ_{ci} (adjusted, MPa)	2	15	10
m_i (feltestimat)	7	17	13
m_i (adjusted)	7	10.2	9



Bergmasseparametere

Table 3. GSI estimates for heterogeneous rock masses such as Flysch.

GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos.P and Hoek. E, 2000)		SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes)				
COMPOSITION AND STRUCTURE		VERY GOOD - Very rough, fresh unweathered surfaces	GOOD - Rough, slightly weathered surfaces	FAIR - Smooth, moderately weathered and altered surfaces	POOR - Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments	VERY POOR - Very smooth slickensided or highly weathered surfaces with soft clay coatings or fillings
	A. Thick bedded, very blocky sandstone The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.	70	60	A		
	B. Sandstone with thin inter-layers of siltstone		50	B		
	C. Sandstone and siltstone in similar amounts			C		
	D. Siltstone or silty shale with sandstone layers			D		
	E. Weak siltstone or clayey shale with sandstone layers				E	
C,D, E and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H.						
	F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure		30		F	
	G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers				G	
	H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.					H

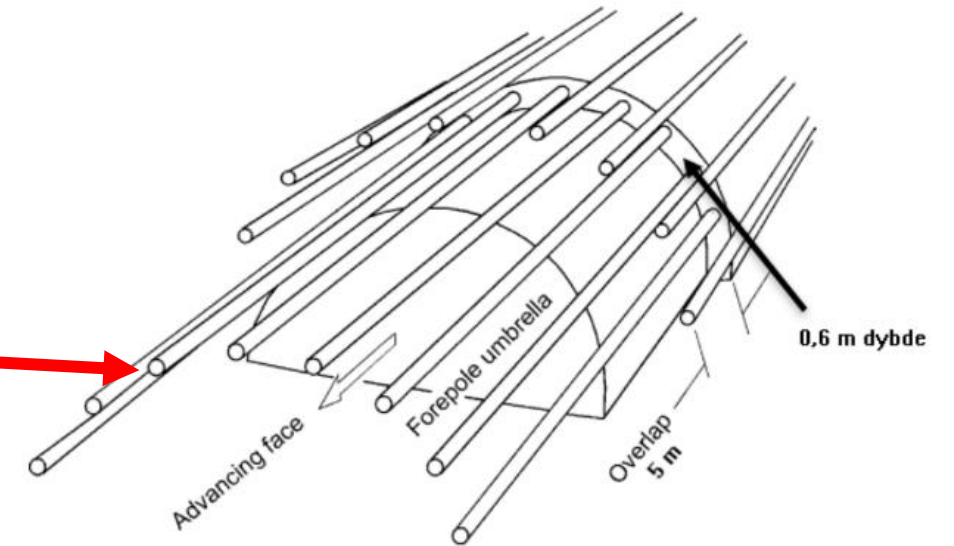
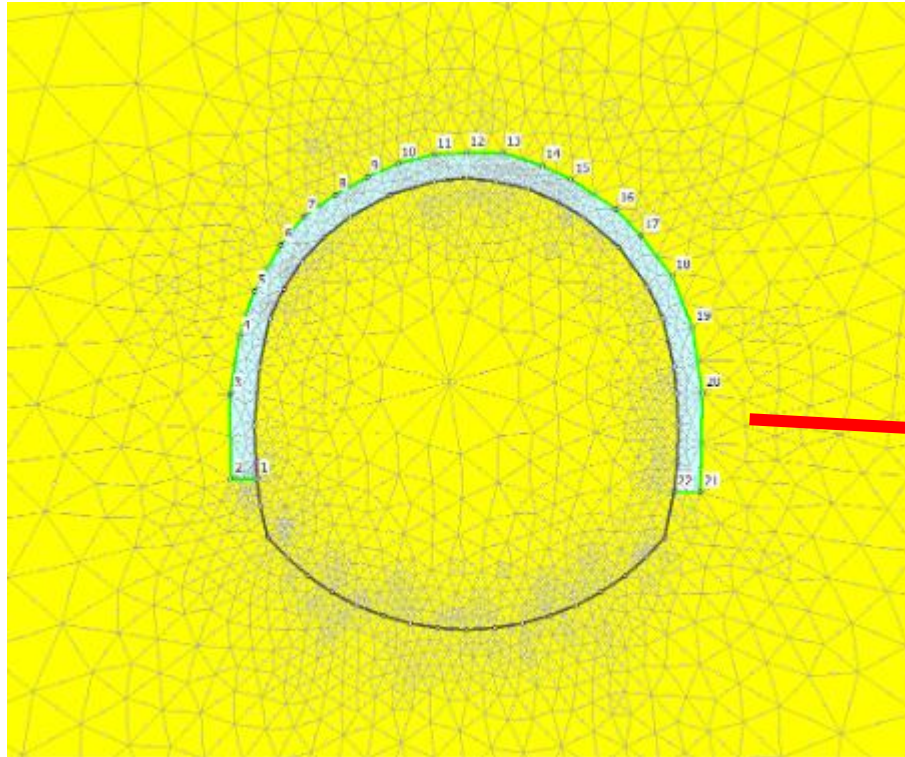
→ : Means deformation after tectonic disturbance

Parameter		Berg i den dårlige sonen	
		Med GSI=20 Konservativ	Med GSI=23 Forvent
Intakt berg	UCS σ_{ci} (MPa)	10	10
	E-modulus (MPa)	20000	20000
Bergmasse	GSI	20	23
	Global bergartsstyrke σ_{cm} (MPa)	0,77	0,85
	m_i	9	9
	m_b	0,52	0,58
	s	0,000138	0,000192
	a	0,54	0,54
	Strekfasthet (MPa)	0,002	0,003
	E-modulus (MPa)	728,98	1069

Marinos & Hoek. 2000. Practical rock engineering

Rørskjerm i sterkt forvitret berg

MULTIC

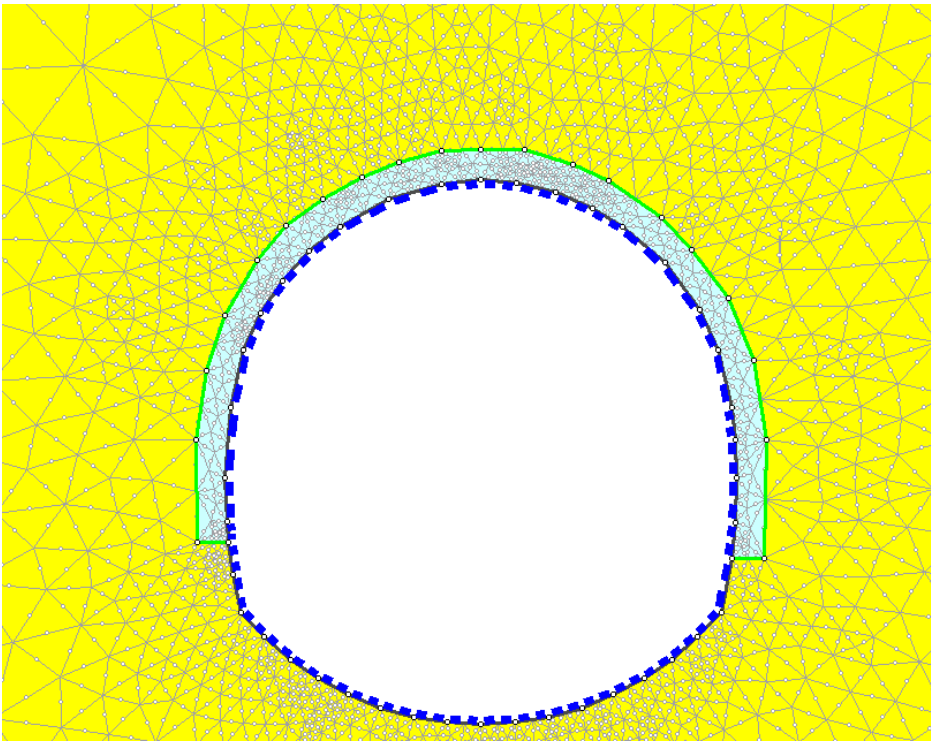


Hoek, Evert. *Numerical Modelling for Shallow Tunnels in Weak Rock*. Upubliserte notater.

Komponent	Areal (m ²)	Styrke (MPa)	Produkt
Bergmasse σ_{cm}	0,6	0,85	0,51
Rørskjerm DP55	0,005	200 [20]	1,1
Injeksjonsmasse RBA 380	0,007	35 [21]	0,2
Sum	0,62	-	1,80
Rørskjermilag σ_{cm} (MPa)	1,80/0,62=2,93		
Rørskjermilag σ_{ci} (MPa)	35		



Bergsikring

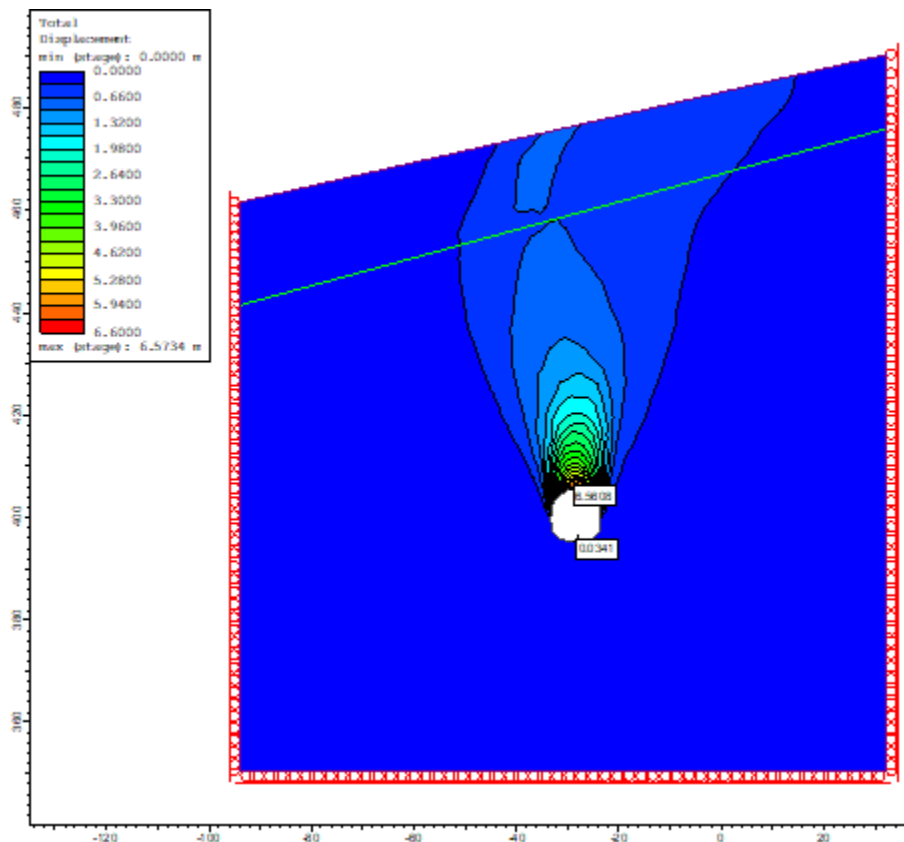


Komponent	Sprøytebetong	Bue	Sprøytebetong over bue
Tykkelse (m)	0,20	6 mm	0,2
E-modulus (MPa)	30000	200000	30000
Poisson ratio	0,15	-	0,15
Trykkfasthet (MPa)	40	400	40
Strekkestyrke (MPa)	3	400	3
Vekt (kg/m)	-	0,44	-
Senteravstand (m)	Under bue, hele profil		Over bue, hele profil

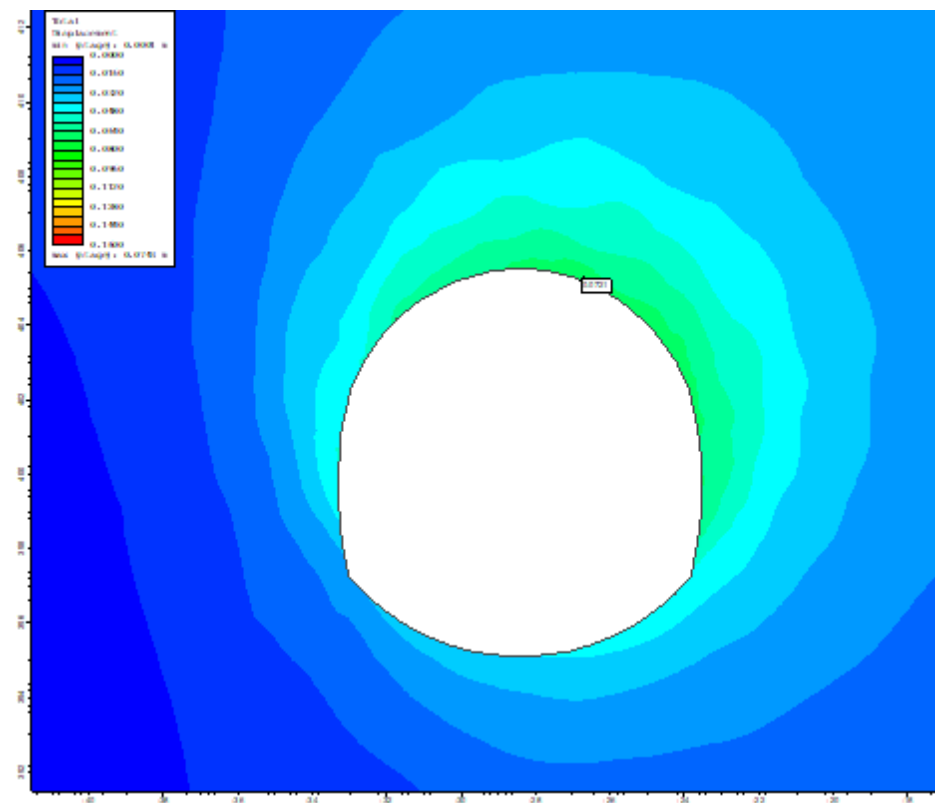


Resultater

- Analysen tilsier at berguttak uten bergsikring fører til svært høy deformasjon



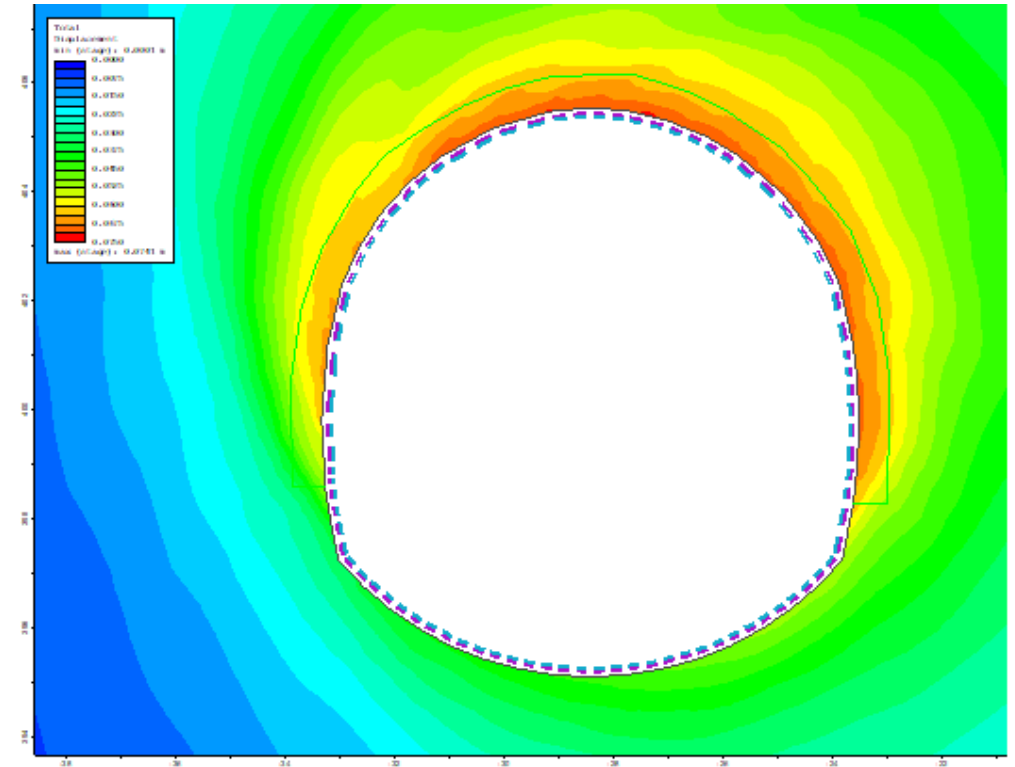
- Med rørskjermlaget reduseres deformasjoner betraktelig





Resultater

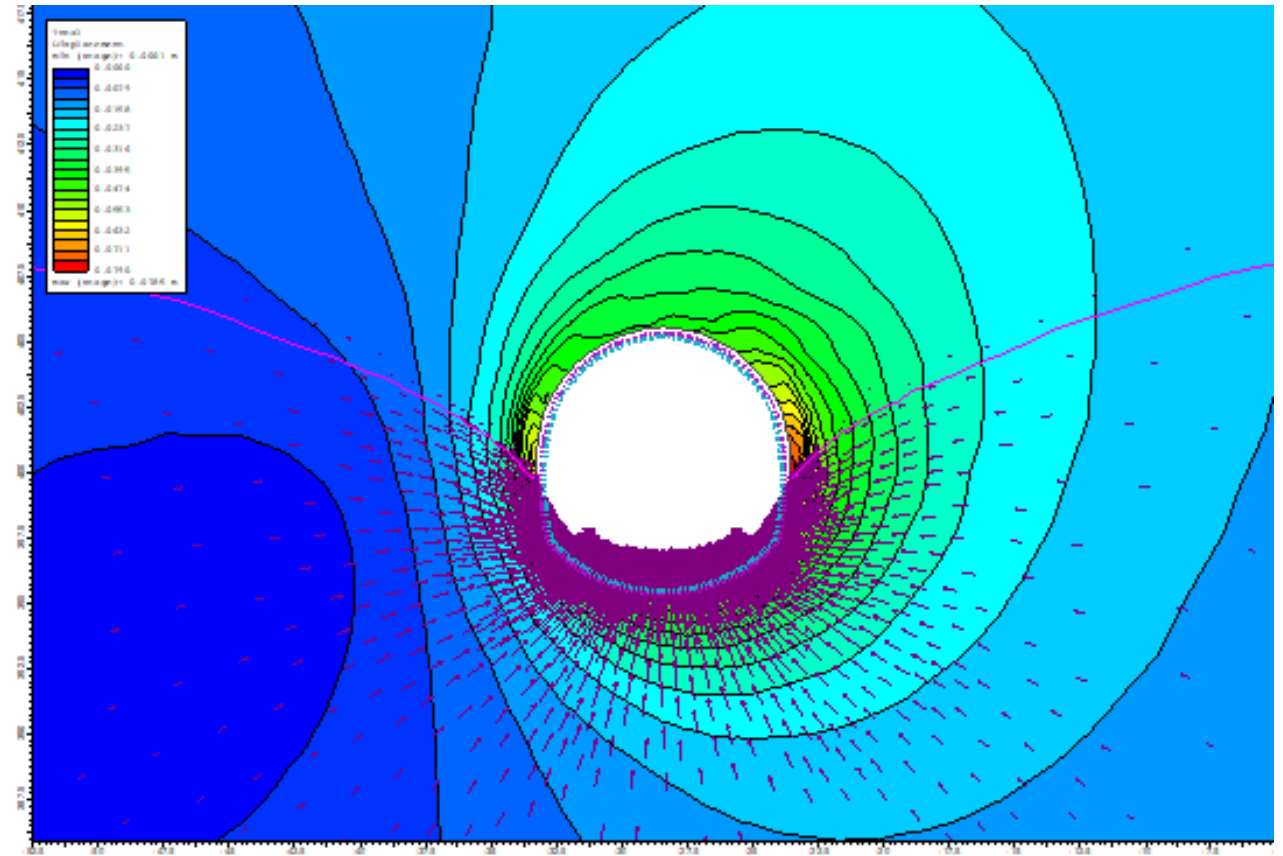
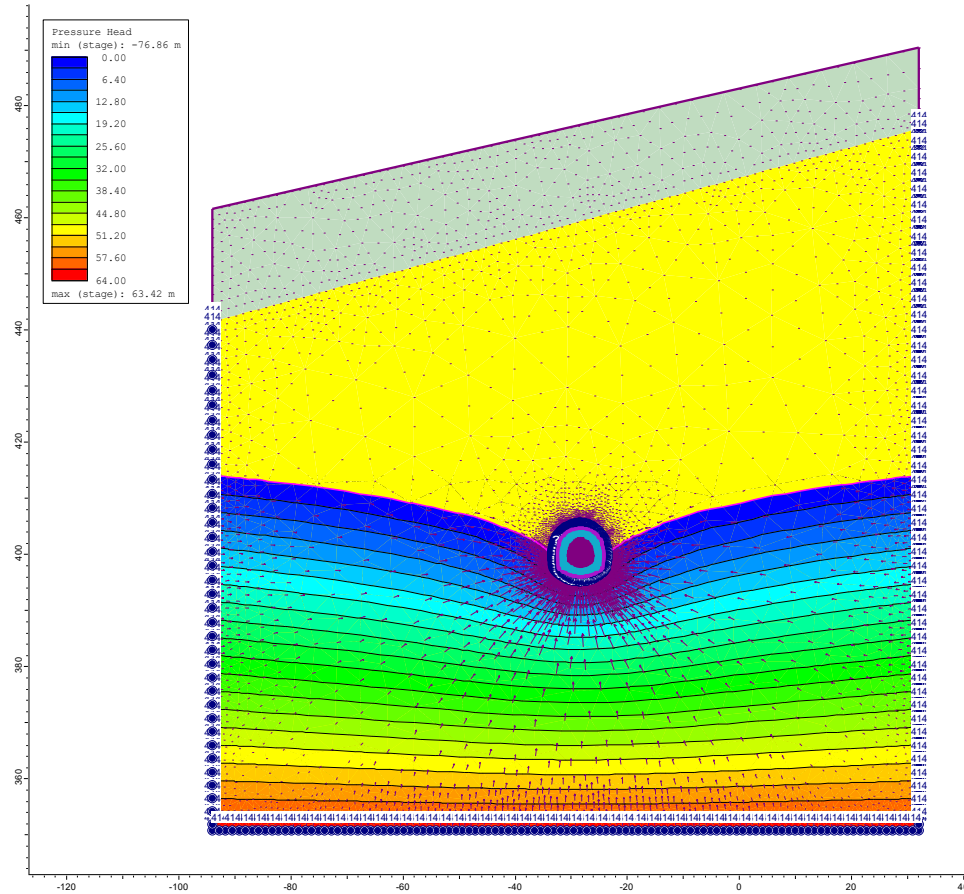
- Stiv bergsikring i lukket ring stopper videre deformasjon
- Sikkerhetsfaktor for bergsikring er tilfredsstillende $>1,4$





Resultater driftfase

- Stabil i driftsfase





Konklusjon

- I denne fasen konkluderer vi med at tunnelen kan drives med kombinasjon av rørskjerm og konvensjonell bergsikring
- Modellen er GSI sensitiv
- Ved lavere GSI må styrken på rørskjermlaget øke
- Bergsikringen har $SF > 1,4$ også i driftsfase
- Det er fortsatt usikkerheter grunnet manglende informasjon
- Sensitivitetsanalyser øker sikkerheten
- Tilfredsstillende resultater for tidligfasevurdering 😊



Multiconsult

Spesiell takk til Hui Lu og Elisabeth Grasbakken